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THE PUFF AND P PUFF COMPUTER PROGRAMS

Richard N. Brodie
Captain USAF

James W. Aubrey, Jr.

TECHNICAL REPORT NO. AFWL-TR-65-24



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Research and Technology Division
AIR FORCE WEAPONS LABORATORY
Air Force Systems Command
Kirtland Air Force Base
New Mexico

March 1965

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FOREWORD

This report was prepared in support of Project 5710, Task 571015, Program Element 7.60.06.01.5.

Inclusive dates of research were January 1964 through February 1965. The report was submitted by the authors 23 February 1965.

The authors wish to thank Lt. Colonel Ralph H. Pennington for his direction and supervision in the preparation of this report.

This technical report has been reviewed and is approved.

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ABSTRACT

The report describes the one-dimensional Lagrangian hydrodynamics computer program, PUFF. The code is used primarily in the study of X-ray effects. In the past year it has been extensively revised and is now quite different from versions used outside the Air Force Weapons Laboratory. The major calculations in each subroutine are explained with a complete description of all input-output variables. Sample problems with the appropriate data deck are included to allow a user to become familiar with data arrangement and to check the program on his computer.

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SECTION I

INTRODUCTION

The purpose of this report is to provide users of the PUFF code with an explanation of the latest version of the program. Several sample problems are included so that the user may become familiar with data input procedures and, at the same time, calibrate the program for his machine. The sample problems were designed to demonstrate a variety of input conditions and should be examined only in that context.

PUFF is a one-dimensional Lagrangian hydrodynamics program used primarily in the study of X-ray effects. The code uses finite difference methods to solve the equations of hydrodynamics using slab geometry and assuming one-dimensional flow through a 1-centimeter-square pipe (reference 1). One may follow a pressure pulse which is propagated through a sample consisting of up to six separate materials. A grid or mesh is superimposed on the materials in the sample. The grid areas are called zones and the grid lines are called zone boundaries. The mesh is numbered, increasing from left to right. The pressure pulse normally starts from the left and progresses through the mesh to the right. When we speak of the front of the mesh, we are referring to the larger zone numbers. When we speak of the back of the mesh, we are referring to the smaller zone numbers.

The index J is consistently used in the code to denote zone numbers. The materials in the sample are numbered consecutively from left to right. The index M is used when a material number is needed.

The original PUFF was a derivative of a Livermore code (reference 2). Extensive work on PUFF was done at the Air Force Weapons Laboratory and additional work was done under contract by McAllister and Associates, Inc. During this development the code became quite large for its degree of sophistication. Many options as to types of problems run were incorporated and an extremely complicated and time-consuming edit routine was developed. Since this development took place over a span of several years, many different

people made separate changes and no concentrated effort was made to delete options that were no longer used. This made the program almost impossible to use for one not intimately familiar with it.

In January of 1964 it was decided to make a version which would retain the essential elements of PUFF but eliminate all options which were not currently in use; and also to make the input-output as straightforward as possible. The monitor subroutine was eliminated and the edit routine was simplified by using the premise that it is more efficient to dump large amounts of required output on binary tape for later edit and plotting and to print only essential data during problem run time.

Since the code was designed to be driven by one of two dissimilar methods, flyer plate (plate slap) and energy deposition, it was decided that a considerable amount of computer time could be saved if the two options were handled in separate codes. The energy deposition code is now called PUFF and the plate slap code is called P PUFF. A great simplification in FORTRAN coding resulted from this division as well as a reduction in core space and computer time required. During this revision cgs units were incorporated and the equation of state was completely divorced from the hydro loop.

The present code consists of a main program where the hydrodynamics is accomplished and from which the other subroutines are called as needed. Each routine has been extensively rewritten and simplified with the exception of rezone where only minor corrections have been made.

PUFF and P PUFF are essentially the same except for the generator subroutines. The section dealing with the generator subroutine points out the major differences between the program.

SECTION II

MAIN PROGRAM

Variables and counters used only in the main program are initialized there instead of in the generator subroutine. Except for local variables being initialized, all calculations in the main program are contained in the time or cycle loop. The time loop begins with the main hydro loop. This loop starts with the first zone, advances in time all quantities associated with that zone, and proceeds with each zone in sequence until all zones have been advanced to the new time. After the hydro loop is completed, numerous checks are made to determine if the problem is complete, if a rezone is possible, or if one of the edit options is desired. If the problem is not complete, a new time step is calculated, the cycle counter N is advanced by 1, and a new cycle is started.

The velocity U , the ordinate of the zone boundary X , the specific volume V , and the artificial viscosity Q are computed in a standard Lagrangian manner. The pressure P , energy E , and sound speed CS are calculated by use of an interpolation method using values returned from an equation-of-state subroutine. This method was developed at the Air Force Weapons Laboratory and eliminates the requirement that the equation of state be in an analytic form.

A tentative time step is computed using the Courant condition modified for the use of artificial viscosity. The actual time step used is the minimum of the tentative time step, 120 percent of the old time step, or 1 one-hundredth of the energy deposit time.

The Lagrangian edit records the time-pressure history of the first zone in the material to the immediate right (downstream) of the chosen zone boundary. This edit is accomplished in the main program since it is exercised every cycle. The zone designated as a JEDIT is not allowed to collapse in rezone. Experience has shown it best not to designate consecutive zones as JEDITS unless one is very careful with the initial zone size.

SECTION III

GENERATOR

1. Introduction

The generator subroutine is called at the start of a problem to read all input data and initialize quantities needed in the problem. It is arranged in independent segments which are executed sequentially. All input values are printed out as a check of the data arrangement and for future reference.

The zoning for both PUFF and P PUFF is computed using a sequence of geometric progressions. This is accomplished using two sets of variables RZ and NZ. The RZs are the common ratios and the NZs are the zone indexes which terminate each progression.

The only essential difference in the generators of PUFF and P PUFF is that PUFF determines an energy deposit rate SS while P PUFF sets a velocity profile. These items are discussed below.

2. Energy Deposition (PUFF)

The absorption coefficients are computed using the formula

$$\mu = \rho \cdot AA \cdot (h \cdot v)^B .$$

The values of AA and B are input numbers referenced to 1 kev that change with material and absorption edges.

One may use the energy spectrum obtained from a multiple black body source or may input an arbitrary spectrum. The arbitrary spectrum may be described by as many as 109 values of energy and corresponding $h \cdot v$ intervals. PUFF now uses 109 values of $h \cdot v / KT$ in the black body calculations instead of the 100 used in previous versions. This change was made to improve the high energy section of the curve. An energy deposit rate, SS, is computed for each zone using the above values in the standard exponential absorption formula.

3. Plate Slap (P PUFF)

P PUFF is designed to simulate the reactions caused by hitting a stationary plate with a piece of material (the flyer plate) moving at a given velocity

upon impact. The starting conditions for the problem simulate those at the instant of impact.

The velocity of each zone in the flyer plate, excluding the last, is set equal to the input variable UZERO. Provision is made to smear the velocity drop, from UZERO to ZERO, over five zones. The velocity of the first zone in the target is set at an input fraction (UFACE) of the flyer velocity. UFACE is used to match the acoustical impedances of the flyer plate and the target.

It may be computed from $UFACE = \frac{Z_{FP}}{Z_{FP} + Z_T}$, where $Z = \rho_0 \cdot$ sound speed.

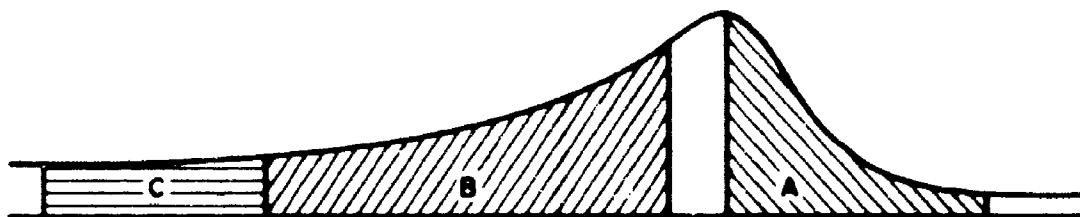
The velocity in the last zone of the flyer plate is the average of the flyer plate velocity and the velocity of the first zone in the target. The velocity of the second zone in the target is one-half that of the first. A print of the calculated velocity profile is given.

SECTION IV
REZONE

1. Introduction

At its best, rezone will introduce small perturbations in the solution. At its worst, rezone can completely destroy a problem. It is hoped that with judicious use the errors introduced will not affect the result by more than a few percent. The computer time saved is substantial.

The rezone routine was designed for a single pulse moving through a mesh having initial zone size increasing with zonal index. Since available computer time limits a problem to a few hundred zones, rezone tries to distribute the zones where they are most needed. The routine attempts to keep the resolution under the pulse constant by reducing zone size as the pressure peak approaches. Certain sections of the mesh are relatively inactive and will allow larger zone sizes. The collapse routine will combine two neighboring zones into one if certain conditions are met. The dividing and combining of zones is done in the divide and collapse routines respectively.



1st zone in mesh expanded less than 20%	1st zone left of max pressure having less than 2/10th max pressure	3rd zone to left of max pressure	zone of max pressure	20th zone in front of zone of max pressure
---	--	----------------------------------	----------------------	--

Figure 1. Rezone Regions

2. Divide Routine

The divide routine operates on twenty zones immediately in front of the zone of maximum pressure (region A, figure 1). To determine an appropriate size for a test zone, the positive momentum of the main pulse and the maximum pressure are used to construct a theoretical triangular pulse which is assumed to be moving with velocity equal to the sound speed of the zone of maximum pressure. The pulse length of this theoretical triangular pulse is found and divided by an input number, ZPUL. This distance is used as the "optimum" zone size in the region. Any zone larger than this check size is divided in half. The divided zone is then checked to see if it should be redivided.

3. Collapse Routine

The collapse routine combines adjoining zones in regions B and C in figure 1. Region B is assumed to be more active than C. Region B extends from three zones to the left of the zone having maximum pressure to the first zone to the left having a pressure less than two-tenths maximum pressure. Region C begins at the left boundary of B and extends to the first zone in the mesh which is expanded less than 20 percent, or to the first zone if no zone is expanded 20 percent. In region B the optimum zone size computed in the divide routine is multiplied by one-half the relative volume (ρ_0/ρ) of the zone of maximum pressure and this quantity is used for the optimum zone size in the region. Each zone in the region smaller than this check size is combined with an adjoining one. Region C uses a rather arbitrarily determined length for its zone size check. The length of the region is divided by the input variable JRZL and used as the optimum zone size. Each zone in the region smaller than this check size is combined with an adjoining zone. Zones designated as material boundaries or JEDITS are not collapsed. The collapse routine is presently entered only once every 100 cycles.

4. Comments

If one is interested in the back part of the mesh (reflected shocks, etc.) at later times, JRZL should be increased to something like 100. A JRZL of 20 will allow very large zones at late times which will effectively damp pulse movement. A ZPUL of 40 is adequate for most problems.

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The divide routine may be bypassed in a problem by initializing ZPUL to zero. The collapse routine may be bypassed in a problem by initializing JRZL to zero.

SECTION V

EDIT

1. Introduction

Elaborate edit routines usually consume a sizable percentage of the computer time used by a problem. This fact leads to a conflict between obtaining sufficient edits to ensure adequate knowledge at all points of interest in the problem and the computer time that is available for the problem. Complicated edit routines also prove difficult in converting from one computer to another.

The present edit routine is divided into two parts. The first part stores, at designated intervals during the problem, all zonal variables and other selected variables on binary tape for later processing. The second part of the routine prints a sufficient number of key variables to enable the user to determine during run time that the problem is progressing satisfactorily, and, after problem completion, to determine points where more detailed edits are wanted. This method has the advantage of using the minimum amount of computer time while providing the maximum amount of available data. It has the disadvantage of requiring the user to wait longer for the final edits and plots.

The Air Force Weapons Laboratory uses the Cal Comp automatic plotter for most PUFF data presentation. The most commonly used plot program simply plots the pressure versus distance for a given time, although more complicated programs exist.

2. Output Variables

All variables printed in the edit routine are defined below.

N	Cycle number.
TIME	Present problem time.
DTNH	Present time step.
JSTAR	Zone number of the last zone in the mesh (from left to right) that has a velocity greater than 10^{-3} cm/sec.

PMAX	The maximum pressure contained in the mesh.
XJPMAX	Coordinate of the zone boundary of the zone having maximum pressure.
JPMAX	Zone number of the zone having the maximum pressure present in the mesh.
MVPULSE	Sum of the momentum of each zone from JPMAX+3 back to the first zone which has a negative velocity.
MVPREC	Sum of the momentum of each zone from JPMAX+4 out to JSTAR+1.
MOMENTUM	Sum of MVPULSE and MVPREC. This expression is computed by averaging the zone mass of two adjoining zones and using the velocity of the boundary between.
DTPP	Pulse width computed using the expression EMVPP/PMAX.
DTPULS	Pulse width computed using the expression EMVPL/PMAX.
ETOTAL	Total energy of the problem, computed by summing the kinetic and internal energy for each zone. The units are calories.
EMVNEG	Total negative momentum in the mesh. This expression is computed by averaging the velocities of two adjacent zone boundaries and using the zone mass of the zone between.
EMVPOS	Total positive momentum in the mesh. This expression is computed by averaging the velocities of two adjacent zone boundaries and using the zone mass of the zone between.
L-BOUND	Coordinate of the left material boundary (X(1)).

X(JBND1)	Coordinate of the boundary between the first and second material. It will be zero for one-material problems.
X(JBND2)	Coordinate of the boundary between the second and third material. It will be zero for two-material problems.
R-BOUND	Coordinate of the right material boundary.
JFIN	Zone number of the last zone in the problem.

SECTION VI
EQUATION OF STATE

1. Introduction

PUFF can now use any equation-of-state subroutine that will return a pressure when presented an energy, density, and material index.

The present equation of state is probably the greatest source of error in PUFF other than rezone. The pressure is computed using one of two functional equations: one for solid regions and one for vapor regions. If the zone is compressed relative to ambient conditions, the solid state equation is used. If the zone is expanded relative to ambient conditions, the vapor state equation is used.

2. Solid Phase

The solid phase equation is based on the Mie-Grüneisen equation of state (reference 3). This equation appears in PUFF as

$$P = C\mu + D\mu^2 + S\mu^3 + G\rho E ,$$

where μ is $\rho/\rho_0 - 1$, G is the Grüneisen parameter and E is energy density. C is determined by the product of ambient density and the weak wave velocity squared. Each of the Hugoniot pressures is multiplied by the expression $(1 - \frac{G\cdot\mu}{2})$ and these points are least squares fit for D and S using C as a known parameter.

3. Vapor Phase

The vapor equation of state is a fit to the Thomas-Fermi-Dirac model in conjunction with a modified γ -law gas equation of state (reference 4).

The equation appears in PUFF as

$$P = n[H + (G-H)n^{1/2}] [E-E_S(1-\exp\frac{N}{n}(1-\frac{1}{n}))] ^{\gamma}$$

where n is ρ/ρ_0 , H is $(\gamma-1)$ effective for small n 's, E_s is the sublimation energy, and N is determined from the expression

$$N = \frac{C}{G(E \cdot \rho_0)} .$$

C , G , and E are defined above.

It is easy to show that the vapor and solid equations have a common limit of $G\rho E$ as the limits $n \rightarrow 1^-$ and $n \rightarrow 1^+$ are taken respectively.

4. Two-Wave Formulation

The most current version of PUFF contains an option for a two-wave structure in the solid phase equation. See figure 2.

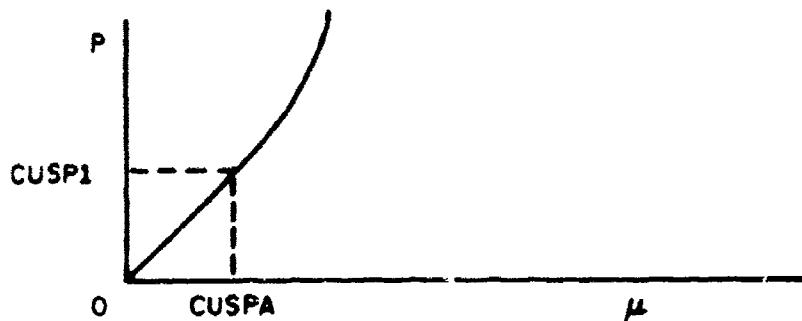


Figure 2. Two-Wave Structure

For μ 's such that $0 \leq \mu \leq \text{CUSPA}$, the pressure is computed by the normal solid equation. For μ 's such that $\text{CUSPA} < \mu$, the pressure is computed using the expression

$$P = \text{CUSPI} + C_1(\mu - \text{CUSPA}) + D_1(\mu - \text{CUSPA})^2 + S_1(\mu - \text{CUSPA})^3 + G \cdot \rho \cdot E .$$

C_1 , D_1 , and S_1 are computed in the same manner as C , D , and S after translating the origin to the point (CUSPA, CUSP1).

SECTION VII

INPUT VARIABLES

This section gives a workable definition of all input variables used in both PUFF and P PUFF. Those followed with a number 1 are used only in PUFF. Those followed with a number 2 are used only in P PUFF. All other variables are common to both codes.

AA(M,I)	(1)	Constants used in computing absorption coefficients. The dimensions are cm^2/gm . See section on Generator subroutine.
ANGLE	(1)	Angle in degrees of the X-ray path measured from the normal of the material. A zero value indicates perpendicular alignment.
B (M,I)	(1)	Dimensionless constants used in computing absorption coefficients. See section on Generator subroutine.
CKP		A problem stop parameter. The problem will terminate when the maximum pressure reaches this distance in centimeters.
CUSPA(M)		$\mu, \frac{P}{P_0} - 1$, corresponding to an inflection point in the Hugoniot data.
CUSPC(M) CUSPD(M) CUSPS(M)		Equation-of-state constants used in the two-wave solid phase equation. The units are dynes/cm^2 . See section on Equation of State.
CUSPG(M)		Grüneisen parameter for the two-wave solid phase equation. It is dimensionless.
CUSPI(M)		Value of the pressure in dynes/cm^2 corresponding to an inflection point in the Hugoniot data.

DISCPT	Description of the problem. Up to 80 permissible Hollerith characters may be used.	
DX	Size of the first zone in centimeters.	
EE(I)	(1)	Total energy in cal/cm ² of each black body. For problems where ANGLE ≠ 0, the total energy for each black body should be multiplied by cos (ANGLE).
EDGE(M,I)	(1)	Values of h·v where the absorption coefficients are discontinuous.
EI(I)	(1)	Energy in cal/cm ² corresponding to each interval of h·v in an arbitrary spectrum problem. For problems where ANGLE ≠ 0, each value of EI should be multiplied by cos (ANGLE). EI is computed in a black body problem.
EQSTC(M) EQSTD(M) EQSTS(M)	{	Equation-of-state constants used in the solid phase equation. The units are dynes/cm ² . See section on Equation of State.
EQSTE(M)		Sublimation energy of material M in ergs/gm.
EQSTG(M)		Grüneisen parameter. It is dimensionless.
EQSTH(M)		(γ-1) effective for low values of p/p ₀ . It is dimensionless.
JBND(M)		Zone number of the last zone in a material (M). The JBND of the last material should be initialized as zero for the code, i.e., JBND (NMTRLS)=0. In a plate slap, if the flyer and target

		are the same material, the JBND(1) = JFIN2.
JCYCS		A problem stop parameter. The problem will terminate after running this many cycles.
JEDIT(I)		Zone number where Lagrangian edits are desired.
JFIN		Zone number of the last zone in the problem.
JRZL		Arbitrary number of zones desired in the collapse region of rezone. Should be 20 to 50 for one-pulse problems, 40 to 100 for two-pulse problems, and 20 to 100 for plate slap problems.
JZPUL		Zoning number used in rezone for di- viding in front of the pulse. A value of 40 is good for all problems. ZPUL is set equal to JZPUL.
LOZHIZ	(1)	Flag used to allow use of rezone in a two-pulse problem. Set to zero for one-pulse problems. Set to 1 if the right pulse is predicted to be dominant in two-pulse problems.
MATL(M)		Material name or description.
NBB	(1)	Number of black bodies used. Should be 1 for an arbitrary spectrum problem
NHNU	(1)	Number of matched values of $h \cdot v$ intervals and energy used in the arbi- trary spectrum input. If zero, used as a flag to select black body energy computation.

NJEDIT		Number of Lagrangian edits selected.
NMTRLS		Number of materials. In a plate slab, if the flyer and target are of the same material, then NMTRLS = 2.
NOE(M)	(1)	Number of edges (discontinuities in absorption coefficients) for each material.
NPRIN		Controls the frequency of printed edits. Edits will be printed at cycles which are integer multiples of this number.
NRZ		Number of zoning ratios used in initial zoning.
NTAPE		Controls frequency of data dumps on binary tape. Information will be stored at cycles which are integer multiples of this number.
NTEDT		Number of time edits selected.
NTEST		A read check variable. Should always be set to 30. If there are too few or too many data cards, the problem will stop.
NZ(I)		Zoning number which changes the zoning ratio (RZ). The code requires this number to be 1 less than the zone where the ratio is wished to be changed.
PMIN(M)		Minimum pressure in dynes/cm ² allowed in the mesh for material M. Approximates the dynamic tensile strength.
RHO(M)		Ambient density in gm/cm ³ of the material M.
RZ(I)		Zoning ratio used in geometrically zoning a problem.

SDUR	(1)	X-ray shine time in seconds.
T(I)	(1)	Temperature in kev of each black body. May be read as zero in an arbitrary spectrum problem.
TBL(I)	(1)	Storage for $h \cdot v / KT$ values for black body problems or $h \cdot v$ values for arbitrary spectrum problems.
TEDIT(I)		Problem times in seconds where edits are desired.
TIME		First time step in seconds. This variable is later used for total problem time. 10^{-12} seconds is a reasonable figure for most problems.
TS		A problem stop parameter. The problem will terminate when TIME reaches this time in seconds.
UFACE	(2)	A constant used to smear the velocity discontinuity between the flyer and the target over five zones. See section on Generator.
UFIN	(2)	Last zone of the flyer plate.
UZERO	(2)	Velocity of the flyer plate.

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APPENDIX I

FORTRAN LISTING OF PUFF

```

PROGRAM PUFF          10
THIS IS PUFF FOR DEPOSITION ONLY FOR THL AFWL 1604 ****      20
                                30
COMMON AA(6,20),AC(10,109,6),B(6,20),CUSPI(6),CUSPA(6),CUSPC(6),      40
1CUSPD(6),CUSPG(6),CUSPS(6),DISCPT(12),EE(10),FDGE(6,20),EI(10,109)      50
2,EQSTC(6),EQSTD(6),EQSTE(6),EQSTG(6),EQSTH(6),EQSTN(6),EQSTS(6),      60
3JBND(6),JEDIT(10),JORG(10),MATL(6),NOE(6),NZ(20),PMIN(6),RHO(6),      70
4RZ(20),SS(801),T(10),TBL(109),TEDIT(25),X(801)      80
                                90
COMMON CKP,DTNH,DTN,JCK,JCYCS,JFIN,JPMAX,JPMAXI,JRL,JSTAR,JXXD,JZ      100
1PUL,LINE,LCZH1Z,N,NBR,NJEDIT,NMTRLs,NPRIN,NRZ,NTAPE,NTEDT,PMAX,      110
2SDUR,TIME,TS,WTAPE,ZPUL      120
                                130
DIMENSION P(1),Q(1),CS(1),E(1),V(1),ZM(1),U(1)      140
                                150
EQUIVALENCE (AC,P),(AC(802),Q),(AC(1603),CS),(AC(2404),E),(AC(3205      160
1),V),(AC(4006),ZM),(AC(4807),U)      170
                                180
ZERODES COMMON      190
DO 1 K=1,9954      200
1 AA(K)=0.      210
CALL GENRAT      220
                                230
INITIALIZE COUNTERS AND CONSTANTS      240
                                250
LINE=0      260
FLAG=0.      270
CC=1.8      280
C1=.25      290
TWOCL=2.*C1      300
COSQ=C0*CO      310
FORCQ=4.*COSQ      320
II=1      330
N=1      340
SSCK=0.      350
DTN=TIME      360
DTNH=TIME      370
HYDRO STARTS HERE      380
                                390
TIME LOOP      400
                                410
SK2M=0.      420
PMAX=0.      430
M=1      440
LL=1      450
DETERMINE THE LEFT BOUNDARY CONDITIONS      460
U(1)=U(1)+DTN*(Q(2)+P(2))/ZM(2)      470
X(1)=X(1)+DTNH*U(1)      480
                                490
MAIN LOOP FOR HYDRO CALCULATION      500

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```

JF INNM=JH IN=1          510
C1=11 J=1+JFINM        520
VOLD=V(J+1)             530
QOL=Q(J+1)              540
PCLD=1(J+1)             550
IF (J+1)=JINM(M1) 4,3,4 560
LL=LL+1                 570
IF (J=J TARI 9,5,6      580
Z(J+2)=MINIF(TIME-UTNH+1,0)*S(J+2) 590
IF (V(J+2)) 7,7,6      600
E(J+1)=V(J+1)           610
GC TO 13                620
LJ=0
CALL WLT(E(J+2)+DL+P(J+1)+LL) 630
U(J+1)=U(J+1)-(UTNH*(P(J+2)+U(J+2)-P(J+1)-U(J+1))/Z(J+1)+ZM(J+1)) 640
IF (U(J+1)-U(J+1)-1.0=-3) 10,10,11 650
U(J+1)=0.0               660
X(J+1)=X(J+1)+(UTNH*U(J+1)) 670
DU=U(J+1)-U(J)           680
V(J+1)=(X(J+1)-X(J))/ZM(J+1) 690
VAVG=(V(J+1)+VOLD)/2.0     700
DV=UTNH*DU/Z(J+1)         710
IF (DU+1.0) 12,13,13     720
J(J+1)=(DU*COSG-C1*CS(J+1))*DU/VAVG 730
IF (J(J+1)-1.0) 13,14,14 740
Q(J+1)=0.0               750
DU=0.0                   760
T(J+1)=0.0               770
IF (TIME->DUR) 14,15,16 780
E(J+1)=E(J+1)+SS(J+1)*UTNH 790
GC TO 18
IF (SSCK) 1H,17,18       800
E(J+1)=E(J+1)+S(J+1)*(SDUR-(TIME-UTNH)) 810
S(J+1)=1.0                820
LNEW=1.0/V(J+1)           830
OLD=E(J+1)                840
CALL LGT(L(J+1)+LNEW+P2+V) 850
L1=P(J+1)+P(J+1)*EV     860
CALL LGST(L1+LNEW+P1+V) 870
L(J+1)=E(J+1)-(P2+P(J+1)+Q(J+1)+VOLD)*DV/(2.0-(P1-P2)/P(J+1)) 880
Q(J+1)=P2+(P2-P1)+(E(J+1)-E(OLD))/POLD/DV 890
DLTD=.001*LNEW            900
IF (DV) 2,19,19            910
DFUDG=DN+V+DLTD          920
GC TO 21
DFUDG=LNEW-LLTD          930
CALL EOST(E(J+1)+DFUDG,PFUDG,M) 940
UPDRHO=(PFUDG-P(J+1))/((DFUDG-DNEW)) 950
IF (DPMRHO) 22,22,27      960
SPEED=1.0                  970
GO TO 24
SPEED=SORTF(UPDRHO)        980
SF 2M1=(SPEED+TWCG1*CS(J+1)-FORCSG*DNU)/(X(J+1)-X(J)) 990
S(J+1)=SPEED
IF (P(J+1)=PMAX) 26,26,26 1000
PMAX=1(J+1)                1010

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26 JMAX=J+1
27 IF (SK2M-SK2M1) 27,27,28
28 SK2M=SK2M1
29 M=LL
30 IF (U(J+1)) 33,29,33
31 IF (N-1) 30,30,31
32 JMAX1=JMAX+1
33 IF (LOZHIZ) 31,32,31
34 IF (U-JSTAR) 33,32,32
35 JSTAR=J
36 GO TO 34
37 CONTINUE
38
39          MAIN LOOP ENDS HERE
40
41 JSTAR=JFINM1
42
43 EXIT AND EDIT CONTROL
44
45 IF (TIME-TS) 35,37,37
46 IF (N=JCYCS) 36,37,37
47 IF (X(JMAX)-CKP) 41,37,37
48 FLAG=1.
49 WTAPE=1.
50 CALL EDIT
51 END FILE 4
52 END FILE 6
53 REWIND 4
54 REWIND 6
55 IF (FLAG) 39,40,39
56 REWIND 45
57 STOP
58 CALL DOTF
59 PAUSE
60 IF (SENSE SWITCH 2) 42,44
61 PRINT 43,N
62 FORMAT (31H SENSE SWITCH 2 IS ON AT CYCLE 110)
63 GO TO 38
64 IF (XMODE(N,NTPA)) 46,45,46
65 WTAPE=1.
66 CALL EDIT
67 GO TO 48
68 IF (XMODE(N,NPRIN)) 46,47,48
69 WTAPE=1.
70 CALL EDIT
71
72          CYCLE ADVANCE
73
74 SK2M=MIN(1,.9/SK2M,1+2*DTNH)
75 IF (NJEDIT) 49,51,49
76 WRITE TAPE 4,NJEDIT,N,TIME
77 DO 50 I=1,NJEDIT
78  JB=JEDIT(I)
79  WRITE TAPE 4,JORG(I),JFCIT(I),P(JB+1)
80  IF (SDUR-TIME) 53,53,52
81  SK2M=MIN(1,.01*SDUR,SK2M)
82  DTNE=DTNH
83  DTNH=SK2M
84  CALL REZONE

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	IF (TEDIT(11)) < 8.58.54	1650
24	IF (NTEDT) 55.57.55	1660
25	IF (TIME+DTNH-TEDIT(11)) 58.58.56	1670
26	DTNH=TEDIT(11)-TIME	1680
	NTEDT=	1690
	GO TO 58	1700
27	WTAPE=1.	1710
	CALL EDIT	1720
	II=II+1	1730
	NTEDT=1	1740
28	TIME=TIME+DTNH	1750
	DTN=DTN+DTNH	1760
	N=N+1	1770
29	IF (DTNH) 59.59.2	1780
	PAUSE25	1790
	GO TO 2	1800
	END	1810

GENERATOR SUBROUTINE FOR THE PUFF HYDRO CODE 1820
 SUBROUTINE GENRAT 1830
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 COMMON AA(6,20),AC(10,109,6),B(6,20),CUSP1(6),CUSPA(6),CUSPC(6),
 1CUSPD(6),CUSPG(6),CUSPS(6),DISCPT(12),EE(10),EDGE(6,20),E1(10,109) 1860
 2EQSTC(6),EQSTD(6),EQSTE(6),EQSTG(6),EQSTH(6),EQSTN(6),EQSTS(6), 1870
 3JBND(6),JEDIT(10),JORG(10),MATL(6),NCE(6),NZ(20),PMIN(6),RHO(6), 1880
 4RZ(20),SS(801),T(10),TBL(109),TEDIT(25),X(801) 1890
 1900
 COMMON CKP,UTNH,DTN,JCK,JCYCS,JFIN,JPMAX,JPMAX1,JRZL,JSTAR,JXXO,JZ 1910
 1PUL,LINE,LOZHIZ,N,NBB,NJEDIT,NMTRLs,NPRIN,NRZ,NTAPE,NTEUT,PMAX, 1920
 2SDUR,TIME,TS,WTAPE,ZPUL 1930
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 DIMENSION P(1),U(1),CS(1),E(1),V(1),ZM(1),U(1) 1950
 EQUIVALENCE (AC,P),(AC(802),Q),(AC(1603),CS),(AC(2404),E),(AC(3205 1960
 1),V),(AC(4006),ZM),(AC(4807),U) 1970
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      REAL 2,NHNU,NTEDT,NJEDIT,L02H12          1.0
      IF (NHNU) 29,30,29          400
 20    READ 4,(TBL(I),E1(I,I),I=1,NHNU)        410
      GO TO 31          420
 21    READ 3,(TBL(I),I=1,109)        430
 22    READ 1,(DISCPT(I),I=1,10)        440
      IF(NTEDT) 33,33,32        450
 23    READ 3,(TEDIT(I),I=1,NTEDT)        460
 24    IF(NJEDIT) 35,35,34        470
 25    READ 2,(JEDIT(I),I=1,NJEDIT)        480
 26    READ 2,NB3,NRZC,NMTRLS,JRZL,JZPUL,NPRIN,NTAPE
      ZPUL=JZPUL        490
 27    READ 3,ANGLE        500
      NMTRLS=1        510
 28    READ 2,(NOE(M),M=1,NMTRLS)        520
 29    READ 3,SDUR,(T(L),EF(L),L=1,NBB)        530
      IF (NMT) 37,37,36        540
 30    READ 2,(JSND(M),M=1,NMT)        550
 31    READ 2,JFIN,(NZ(L),L=1,NRZC)        560
 32    READ 3,DX,TIME,(RZ(M),M=1,NRZC)
      DX=DX/RZ(1)        570
 33    DO 38 M=1,NMTRLS        580
 34    READ 1,MATL(M)        590
 35    READ 3,RHO(M),EQSTC(M),EQSTD(M),EQSTE(M),EQSTG(M),EQSTH(M),EQSTS(M)
      ,PMIN(M)        600
 36    REAL 3,CUSPI(M),CUSPA(M),CUSPC(M),CUSPD(M),CUSPG(M),CUSPS(M)
      EQSTN(M)=EQSTC(M)/EQSTG(M)/(EQSTE(M)*RHO(M))        610
 37    NOED=NCE(M)        620
 38    READ 3,(AA(M+1),B(M+1),EDGE(M+1),I=1,NCED)        630
 39    READ 3,CKP,T5        640
 40    READ 2,JCYCS,NTEST        650
      IF (NTEST-30) 39,40,32        660
 41    PRINT 7        670
 42    STCP        680
 43    JKCK=0        690
 44    JXXO=0        700
 45    NRZ=-5        710
 46    ANGLE=COS(ANGLE/57.2957795)        720
 47    IF(NJEDIT) 43,4,41        730
 48    DO 42 I=1,NJEDIT        740
 49    JORG(I)=JEDIT(I)        750
 50
 51          CALCULATE ABSORPTION COEFFICIENTS        760
 52
 53    IF(NHNU) 44,50,44        770
 54    DO 48 M=1,NMTRLS        780
 55    K=1        790
 56    DO 48 I=1,NHNU        800
      IF (EDGE(M,K)-TBL(I)) 46,46,47        810
 57    K=K+1        820
 58    GO TO 45        830
 59    AC(I,I,M)=-RHC(M)*AA(M,K)*(TBL(I)**B(M,K))/ANGLE        840
 60    CONTINUE
 61    EITOT=0
 62    DO 49 I=1,NHNU
 63    EITOT=EITOT+E(I,I)
 64    GO TO 59

```

```

50   EITOT=0.
      DO 54 M=1,NMTRLS
      DO 54 L=1,NBB
      K=1
      DO 54 I=1,109
      51   IF (EDGE(M,K)-TBL(I)*T(L)) 52,52,53
      52   K=K+1
      GO TO 51
      53   AC(L,I,M)=-RHO(M)*AA(M,K)*(TBL(I)*T(L))**B(M,K)/ANGLE
      54   CONTINUE
      DO 57 L=1,NBB
      DO 57 I=1,109
      IF (I=99) 55,55,56
      55   EI(L,I)=EE(L)*.01
      GO TO 57
      56   FI(I,I)=EE(L)**.001
      57   CONTINUE
C
C           COMPUTE DX USING ZONEING CONSTANTS
C
      58   LZ=1
      DO 61 J=1,JFIN
      IF (J=1-NZ(LZ)) 60,59,60
      59   LZ=LZ+1
      60   DX=DX*RZ(LZ)
      61   X(J+1)=X(J)+DX
C
C           ZONE DEPOSITION
C
      M=1
      DO 71 J=1,JFIN
      ESUM=C.
      IF (J=JBND(M)) 63,62,63
      62   M=M+1
      63   IF (NHNU) 64,67,64
      64   DO 66 I=1,NHNU
      IF (EI(1,I)-1.E-20) 66,65,65
      65   EIZ=EI(1,I)*(1.-EXP(-AC(1,I,M)*(X(J+1)-X(J))))
      EI(1,I)=EI(1,I)-EIZ
      ESUM=ESUM+EIZ
      66   CONTINUE
      GO TO 70
      67   DO 69 L=1,NBB
      DO 69 I=1,109
      IF (EI(L,I)-1.E-20) 69,68,68
      68   EIZ=EI(L,I)*(1.-EXP(-AC(L,I,M)*(X(J+1)-X(J))))
      EI(L,I)=EI(L,I)-EIZ
      ESUM=ESUM+EIZ
      69   CONTINUE
      70   SS(J+1)=ESUM*4.186E7/RHO(M)/(X(J+1)-X(J))/SDUR
      IF (SS(J+1)-1.E12/RHO(M)) 72,71,71
      71   CONTINUE
C
C           CLEAR STORAGE TO ZERO FOR HYDRO
C
      72   DO 73 I=1,560P
      AC(I)=C.

```

Best Available Copy

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```

```

16 IF (J-(J-NM(M))+1) .LT. 186,87      4100
17 M=M+1
18 IF (OPT1*ICSTK(M)-1.0E-7) .NE. 0.000000      4110
19 IF (OPTAR1) 89,81,90      4120
20 81 TAU=0.0
21 82 X=X(J)+X(J-1)
22 ERCPA=ERPG*RHD(M)*DX      4130
23 CALPA=ERPA*1.0E-7/4.186      4140
24 SUMCAL=RUMCAL+CALPA      4150
25 PRINT 24,J,DX,X(J),ERCPA,CALPA,RUMCAL,HPC,X(J),ZM(J),J      4160
26 IF (XVODE(J,10)) 92,91,92      4200
27 PRINT 22,(OPT(I),I=1,10)      4210
28 CONTINUE
29 IF (OPTAR1) 83,83,84      4230
30 83 TAU=0.01N
31 PRINT 26
32 RETURN
33 END

```

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SETTING UP ZONE FOR THE DUFF HYDRO CODE

4140

AHEAD TIME BEZONING

4150

1000000 AA(6,20),AC(10,10P+6),B(6,20),CUSPI(6),CUSPA(6),CUSPC(6),
 CUSPG(6),CUSPG(6),CUSTG(6),CISCP(12),EE(10),EDGF(6,20),E(110,10+1),
 E05T(6),EGSTF(6),EGSTE(6),EGSTG(6),EGSTH(6),EGSTN(6),EGSTS(6),
 ER(6),ERDIT(10),ERFC(10),ERATL(6),NDE(6),NZ(20),PMIN(6),RHO(6),
 RPP(6),RPT(6),T(12),TH(1,12),TEDIT(20),X(80)

4160

1000000 CEF, TMU, TNU, UCYC, UF IN, UPMAX, UPMAXI, JRZL, JSTAR, UXXG, UY
 UYLEV, UYLOZMIZ, UYNU, UYNUEDIT, NMTRLS, NPRINT, NRZ, INTAPE, PMAX,
 PMAXI, TNU, UYNU, UYNU

4170

1000000 P(1),V(1),CS(1), (1),V(1),ZM(1),U(1)

4180

1000000 EQUIVALENCE (AC,P)+(AC(802)+Q)+(AC(1603)+S)+(AC(2404)+E)+(AC(3204)
 +(AC(4004)+W)+(AC(4807)+U)

4190

FORMAT (F10.3,4110)

4200

BEZONING AHEAD OF MAIN PRESSURE PULSE

4210

CONTINUE
 UTPRF=1
 IF (UPMAX-UZPUL-JRZL-UPMAXI) = 87,87+2
 UY=1
 NE1
 DO 6 J=1,JSTAR
 IF (J=JPNL(M)) = 4,3+4
 M=M+1
 IF (RHO(Y)*V(J+1)-1.2) = 7.5+5
 UY=0
 CONTINUE
 IF (ZPUL) = 48+48+8
 UY=UPMAX+3
 XUPMAX=Y(UPMAX)
 ENVPRL=0
 ENVPRL=ENVPRL+U(Y)*.5*(ZM(JM+1)+ZM(JM))
 IF (U(JM+1)) = 12+12+10
 IF (JM+1) = 12+12+11
 UY=JM+1
 DO TC = 0
 UY=UPMAX+4
 ENVPRL=0
 ENVPRL=ENVPRL+U(Y)*.5*(ZM(JM)+ZM(JM+1))
 IF (JM=JSTAR) = 14+14+15
 UY=JM+1
 DO TC = 12
 ENVPRL=ENVPRL+U(Y)
 UTPRF=ENVPRL/PMAX
 R2=X=2,* UTPRF*ENVPRL/UPMAX+ZPUL
 J=JUPMAX
 UY=1
 IF (J+1)=JFTN = 17+48+48
 IF (X(J+1)-Y(J+1)-R2*X) = 18+18+19

4220

4230

4240

4250

4260

4270

4280

4290

4300

4310

4320

4330

4340

4350

4360

4370

4380

4390

4400

4410

4420

4430

4440

4450

4460

4470

4480

4490

4500

4510

4520

4530

4540

4550

4560

4570

4580

4590

4600

4610

4620

4630

4640

4650

4660

4670

4680

4690

4700

4710

4720

4730

4740

4750

4760

4770

4780

4790

4800

4810

4820

4830

4840

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```

18 IF (J=JPMAX+20) 16,48,48 4850
19 IF (J=JXX0) 48,48,20 4860
20 CALL EDIT 4870
SCRNCH=1.
JFINO=JFIN 4880
JXX0=J 4890
DO 22 MCK=1,NMTRLS 4900
IF (J=1-JBND(MCK)) 23,21,22 4910
21 JCK=MCK 4920
22 CONTINUE 4930
MCK=NMTRLS 4940
ME=MCK 4950
23 ME=MCK 4960
24 IF (JCK) 25,25,26 4970
25 RZR=.5*(X(J-1)+X(J))-X(J-2))/(X(J)-X(J-2)) 4980
EL=E(J-1)+RZR*(E(J)-E(J-1)) 4990
VL=V(J-1)+RZR*(V(J)-V(J-1)) 5000
SSL=SS(J-1)+RZR*(SS(J)-SS(J-1)) 5010
IF (J=JBND(ME)) 26,27,26 5020
26 RZR=(X(J+1)-.5*(X(J)+X(J-1)))/(X(J+1)-X(J-1)) 5030
ER=E(J+1)+RZR*(E(J)-E(J+1)) 5040
VR=V(J+1)+RZR*(V(J)-V(J+1)) 5050
SSR=SS(J+1)+RZR*(SS(J)-SS(J+1)) 5060
IF (JCK) 29,29,28 5070
27 RZR=.5*(X(J)-X(J-1))/(X(J)-X(J-2)) 5080
ER=E(J)+RZR*(E(J)-E(J-1)) 5090
VR=V(J)+RZR*(V(J)-V(J-1)) 5100
SSR=SS(J)+RZR*(SS(J)-SS(J-1)) 5110
GO TO 29 5120
28 RZR=.5*(X(J)-X(J-1))/(X(J+1)-X(J-1)) 5130
EL=E(J)+RZR*(E(J)-E(J+1)) 5140
VL=V(J)+RZR*(V(J)-V(J+1)) 5150
SSL=SS(J)+RZR*(SS(J)-SS(J+1)) 5160
29 XR=X(J) 5170
XL=.5*(X(J)+X(J-1)) 5180
ZMR=(XR-XL)/VR 5190
ZML=(XR-XL)/VL 5200
UR=U(J) 5210
UL=((ZM(J)-ZML)*U(J-1)+(ZM(J)-ZMR)*U(J))/(ZML+ZMR) 5220
DEN=1./VL 5230
CALL EGST (EL,DEN,PL,ME) 5240
DEN=1./VR 5250
CALL EGST (ER,DEN,PR,ME) 5260
QL=G(J) 5270
QR=G(J) 5280
CSL=CS(J) 5290
CSR=CS(J) 5300
JDO=J 5310
JI=ME 5320
DO 31 NME=JDO+JFIN 5330
IF (NME=JBND(J)) 31,30,31 5340
30 JBND(J)=NME+1 5350
JI=JI+1 5360
31 CONTINUE 5370
JXX=J 5380
J=JFIN 5390
32 X(J+1)=X(J) 5400
U(J+1)=U(J) 5410

```

```

    ZM(J+1)=ZM(J)          440
    V(J+1)=V(J)            440
    E(J+1)=E(J)            440
    P(J+1)=P(J)            440
    Q(J+1)=Q(J)            440
    CS(J+1)=CS(J)          440
    S(J+1)=S(J)            440
    J=J-1                  440
    IF (J-JXX) 33,33,32
33   X(J+1)=XR
    X(J)=XL
    U(J+1)=UR
    U(J)=UL
    ZM(J+1)=ZMR
    ZM(J)=ZML
    V(J+1)=VR
    V(J)=VL
    E(J+1)=ER
    E(J)=EL
    P(J+1)=PR
    P(J)=PL
    Q(J+1)=QR
    Q(J)=QL
    CS(J+1)=CSR
    S(J)=CSL
    S(J+1)=SSR
    S(J)=SSL
    IF(NJEDIT) 37,37,34
34   SC ME II=1,NJEDIT
    IF(J-JEDIT(II)) 35,35,36
35   JEDIT(II)=JEDIT(II)+1
36   CONTINUE
37   IF(J-JSTAR) 38,38,39
38   JSTAR=JSTAR+1
39   JFIN=JFIN+1
    IF (J1-X(J)-X(J-1)-RZDX) 40,24,24
40   IF (J-JXX0-20) 41,47,47
41   J=J+2
    IF (J-JFIN) 42,47,47
42   IF (E(J+1)) 43,43,44
43   E(J+1)=MIN(F(TIME-DTNH,ENDT)*SE(J+1)
44   IF (J1-JBND(MF)) 45,46,45
45   JKCK=0
    GO TO 25
46   MF=MF+1
    JKCK=1
    SC TC 26
47   JRZ=JFINC-JFIN
    PRINT 1,TIME,N,JRZ,JSTAR
    REZONE BEHIND MAIN PRESSURE PULSE
48   IF (JRZL) 87,87,49
49   IF (N-NRZ-100) 87,87,50
50   JRZV=1
    MR7=1
    JFINO=JFIN

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```

      IF (INS>UFTN+1)          5990
      M=WRZ                      6000
      KRZ=1                      6010
      UJUMAX                     6020
      UJV=1                      6030
      IF ((P(0))/PMAX=.2) 52,52,51 6040
      UPLC=0                      6050
      IF ((UPLC-UV-JRZL)) 53,53,60 6060
      3  IF ((URMAX-UPLC-UZRUL)) 54,54,65 6070
      4  IF ((KRZ)) 57,57,56 6080
      5  UJULC=1                  6090
      DO 56 MM=1,NMTRLS          6100
      16  IF (UJULC+1)=MM(MM)) 57,57,56 6110
      CONTINUE                    6120
      NMENMTRLS                  6130
      17  MM=M                      6140
      DO 54 MM=1,NMTRLS          6150
      18  IF ((URMAX-UJND(MM))) 59,59,59 6160
      CONTINUE                    6170
      NMENMTRLS                  6180
      19  RZR=ZRXX*.5*(URMAX)*RHOC(MM) 6190
      KRZ=-1                     6200
      GO TO 63                     6210
      KRZ=1                     6220
      DO 61 MM=1,NMTRLS          6230
      19  IF (UV+1-UJND(MM)) 62,62,61 6240
      CONTINUE                    6250
      NMENMTRLS                  6260
      20  MM=M                      6270
      RZR=(X(UPLC)-Y(UV))/FLOATE(UZRUL) 6280
      UJV+=1                     6290
      21  IF (SCPNCH) 64,64,65          6300
      CALL EDIT                    6310
      SCRNCHE=1                   6320
      22  IF ((X(J+1)-Y(J)-RZR)) 66,61,61 6330
      23  IF ((J+1)-UJND(M)) 67,61,67 6340
      24  IF ((NU-M)) 70,70,68 6350
      25  DO 11 J=1,NJEDIT          6360
      11  IF ((J+1)-JEDIT)) 69,61,69 6370
      CONTINUE                    6380
      26  ZMINV=1./((ZM(J+1)+ZM(J+2)) 6390
      27  U(J+1)=(U(J+1)+ZM(J+1)+ZM(J+2)*Z*(J+2))*ZMINV 6400
      V(J+1)=(V(J+1)+ZM(J+1)+V(J+2)*ZM(J+2))*ZMINV 6410
      E(J+1)=(E(J+1)+ZM(J+1)+E(J+2)*ZM(J+2))*ZMINV 6420
      DEN=1./V(J+1)                6430
      CALL EDIT ((J+1),VENHIC(J+1),M) 6440
      DA=(ZM(J)+U(J+2)*U(J+1)*(U(J)+U(J+1)))/(ZM(J)+2.*ZM(J+1)) 6450
      ZM=ZM(J+2)+2.*ZM(J+2)          6460
      28  IF ((ZM)) 71,72,71          6470
      29  U=1.2*(U+2)*U(J+2)+ZM(J+2)*(U(J+2)+U(J+1))/ZMC 6480
      GO TO 73                      6490
      30  UJ=0                      6500
      31  ZA(J+1)=V(J+1)+ZM(J+2)          6510
      32  U(J+1)=(U(J+1)+U(J+2))/2.0 6520
      U(J+1)=U(J+1)+E(J+2)/ZM(J+2) 6530
      U(J)=U(J) 6540
      U(J+1)=U(J) 6550

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X(J+1)=X(J+2)          6560
JX=J+2                  6570
DO 74 JC=JX,JFINC      6580
X(JC)=X(JC+1)          6590
U(JC)=U(JC+1)          6600
ZM(JC)=ZM(JC+1)        6610
V(JC)=V(JC+1)          6620
E(JC)=E(JC+1)          6630
P(JC)=P(JC+1)          6640
Q(JC)=Q(JC+1)          6650
CS(JC)=CS(JC+1)        6660
SS(JC)=SS(JC+1)        6670
CONTINUE                6680
JFIN=JFIN-1            6690
IF (NJEDIT) 78,78,75
74 DO 77 I=1,NJEDIT      6700
     IF (I-JFEDIT(I)) 76,77,77
75 NJEDIT(I)=JFEDIT(I)-1   6710
76 CONTINUE                6720
77 JMAX=JMAX-1            6730
78 CONTINUE                6740
JSTAR=JSTAR-1            6750
JPLC=JPLC-1              6760
JXX0=JXX0-1              6770
DO 80 M=1,NMTRS          6780
     IF (JBND(M)-J-2) 80,79,79
80 JBND(M)=JBND(M)-1      6790
CONTINUE                6800
END COLLAPSE             6810
81 IF (<R7) 83,87,82      6820
82 IF (J-JPLC) 84,83,83      6830
83 IF (J+4-JMAX) 84,86,86      6840
84 J=J+1                  6850
     IF (J-JBND(M)) 65,85,85
85 M=M+1                  6860
CONTINUE                6870
86 GO TO 65                6880
87 JRZ=JFIN-JFIN          6890
JMAXI=JMAXI-JRZ          6900
NRZ=N                    6910
PRINT I,TIME,N,JRZ,JSTAR      6920
CONTINUE                6930
88 IF (<CNCNCH) 89,89,88      6940
CALL ETIT                  6950
89 RETURN                  6960
90 END                      6970
91 RETURN                  6980
92 END                      6990

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      U=0.5*(X(1)+X(2))
      VPL=0.
1.   S1=VPL+(VPL+U(JM))*0.5*(ZM(JM+1)+ZM(JM))    7570
      IF (JM-JMAX) 13,14,14
13   IF (U(JM-1)) 16,16,14
14   IF (U(JM-1)) 16,16,15
15   JM=JM-1
16   GO TO 12
17   J*=JMAX+4
      EMVPOS=0.
18   EMVPOS=(VPPR+U(JM))/2.0*(ZM(JM)+ZM(JM+1))    7600
      IF (JM-JSTAR) 18,19,19
19   JM=JM+1
20   GO TO 17
21   J=J+4*EMVPL+EMVPR
      EMVPR=VPPR/HMAX
      DTPL=EMVPL/PMAX
22   PRINT OUTPUT VARIABLES
      J=J+1,JBND(1)
      J=J+JBND(2)
23   PRINT 1,N,TIME,LTRN,H,JSTAR,JMAX,PMAX,XPMAX,EMVPL,EMVPR,EMVPP,DTPL
      1,N,TOTAL,S,EMNEG,EMVPOS,X(1),X(JBND1),X(JBND2),X(JFIN),JFIN
      LTRN=LTIN+R
      1,XXCODE(LTNE,SC) 21,20,21
24   PRINT ?
25   RETURN
26   END

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APPENDIX II

FORTRAN LISTING OF P PUFF

```

C PROGRAM P PUFF
C THIS IS PUFF FOR PLATE SLAPS ONLY FOR THE AWFL 1604 *****
COMMON CS(500),CUSP1(6),CUSPA(6),CUSPC(6),CUSPD(6),CUSPG(6),
1 CUSPS(6),DISCPT(12),E(500),EQSTC(6),EQSTD(6),EQSTE(6),EQSTG(6),
26),EQSTH(6),EQSTN(6),EQSTS(6),JBND(6),JEDIT(10),JORG(10),MATL(6),N
3Z(20),P(500),PMIN(6),Q(500),RHO(6),RZ(20),TEDIT(25),U(500),V(500),
4X(500),ZM(500)                                     10
C
C COMMON CKP,DTN,DTNH,JCK,JCYCS,JFIN,JFIN2,JPMAX,JRZL,JSTAR,JXXC,JTF
IUL,LINE,N,NJEDIT,NMTRL5,NPRIN,NRZ,NTAPE,NTEDT,PMAX,TIME,TS,UZERO,
2WTAPE,ZPUL                                         110
C
C ZEROES COMMON
C
C DO 1 K=1,4225
1 CS(K)=0.
CALL GENRAT
C
C          INITIALIZE COUNTERS AND CONSTANTS
C
LINE=0
FLAG=0.
CC=1.8
C1=.25
TWOC1=2.*C1
COSQ=C0*C0
FORCSQ=4.*COSQ
II=1
N=1
DTN=TIME
DTNH=TIME
JSTAR=JBND(1)+3
C
C HYDRO STARTS HERE
C          TIME LOOP
C
2 SK2M=0.
PMAX=0.
M=1
LL=1
C DETERMINE THE LEFT BOUNDARY CONDITIONS
U(1)=U(1)-DTN*(Q(2)+P(2))/ZM(2)
X(1)=X(1)+DTNH*U(1)
C
C          MAIN LOOP FOR HYDPO CALCULATION
C
JFINM1=JFIN-1
DO 22 J=1,JFINM1
QOLD=Q(J+1)
POLD=P(J+1)

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```

VCLD=V(J+1)          1.1
IF (J+1-JBNU(M)) 4,3,4          510
3 LL=LL+1          520
4 U(J+1)=U(J+1)-DTNH*(P(J+2)+Q(J+2)-P(J+1)-S(J+1))/(ZM(J+1)+ZM(J+2))          530
IF (A0SF(U(J+1))-1.E-3) 5,5,6          540
5 U(J+1)=0.0          550
6 X(J+1)=X(J+1)+DTNH*U(J+1)          560
DU=U(J+1)-U(J)          570
V(J+1)=(X(J+1)-X(J))/ZM(J+1)          580
VAVG=(V(J+1)+VOLD)/2.0          590
DV=DTNH*DU/ZM(J+1)          600
IF (DU+1.) 7,8,8          610
7 G(J+1)=(DU*C0SO-C1*C(J+1))*DU/VAVG          620
IF (G(J+1)-1.) 8,9,0          630
8 Q(J+1)=0.0          640
DU=0.0          650
CS(J+1)=0.0          660
9 DNEW=1./V(J+1)          670
EOLD=E(J+1)          680
CALL EQST (E(J+1),DNEW,P2,M)          690
E1=E(J+1)-P(J+1)*DV          710
CALL EQST (E1,DNEW,P1,M)          720
E(J+1)=E(J+1)-(P2+P(J+1)+Q(J+1)+QOLD)*DV/(2.-(P1-P2)/P(J+1))          730
P(J+1)=P2+(P2-P1)*(E(J+1)-EOLD)/POLD/DV          740
DLTD=.C01*DNEW          750
IF (DV) 11,11,10          760
10 DFUDG=DNEW+DLTD          770
GO TO 12          780
11 DFUDG=DNEW-DLTD          790
12 CALL EQST (E(J+1),DFUDG,PFUDG,M)          800
DPDRHO=(PFUDG-P(J+1))/(DFUDG-DNEW)          810
IF (DPDRHO) 13,13,14          820
13 SPEED=C.          830
GO TO 15          840
14 SPEED=SQRTF(DPDRHO)          850
15 SK2M1=(SPEED+TWOCL*CS(J+1)-FORCSO*DU)/(X(J+1)-X(J))          860
CS(J+1)=SPEED          870
C          880
IF (P(J+1)-PMAX) 17,16,16          890
16 PMAX=P(J+1)          900
JPMAX=J+1          910
17 IF (SK2M-SK2M1) 18,18,19          920
18 SK2M=SK2M1          930
19 M=LL          940
IF (U(J+1)) 22,20,22          950
20 IF(J-JSTAR) 22,21,21          960
21 JSTAR=J          970
GO TO 23          980
22 CONTINUE          990
C          1000
MAIN LOOP ENDS HERE          1010
JSTAR=JFINM1          1020
C          1030
C          1040
C          1050
C          1060
23 IF (TIME-TS) 24,26,26          1070
24 IF (N-JCYCS) 25,26,26

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```

23 IF (X(JPMAX)-CKP) 30,26,26          12
26 FLAG=1.                                1150
27 WTAPE=1.                                1160
    CALL EDIT                               1170
    END FILE 4                            1180
    END FILE 6                            1190
    REWIND 4                               11A0
    REWIND 6                               11B0
    IF (FLAG) 28,29,28                   11C0
28 REWIND 45                               11D0
    STOP                                    11E0
29 CALL DOTF                             11F0
    PAUSE                                  1200
30 IF (SENSE SWITCH 2) 31,33              1210
31 PRINT 32,N                            1220
32 FORMAT (31H SENSE SWITCH 2 IS ON AT CYCLE 110) 1230
    GO TO 27                           1240
33 IF (XMODF(N,NTAPE)) 35,34,35        1250
34 WTAPE=1.                                1260
    CALL EDIT                               1270
    GO TO 37                           1280
35 IF (XMODF(N,NPRIN)) 37,36,37        1290
36 WTAPE=0.                                1300
    CALL EDIT                               1310
                                CYCLE ADVANCE
37 SK2M=MIN(1,.8/SK2M,1.2*DTNH)          1320
    IF (NJEDIT) 38,40,38                  1330
38 WRITE TAPE 4,NJEDIT,N,TIME            1340
    DO 39 I=1,NJEDIT                     1350
    JB=JEDIT(I)
39 WRITE TAPE 4,JORG(I),JEDIT(I),P(JB+1) 1360
40 DTN=DTNH                            1370
    DTNH=SK2M                           1380
    CALL REZONE                          1390
    IF (TEDIT(III)) 45,45,41             1400
41 IF (NTEDT) 42,44,42                  1410
42 IF (TIME+DTNH-TEDIT(III)) 45,45,43   1420
43 DTNH=TEDIT(III)-TIME                1430
    NTEDT=0                            1440
    GO TO 45                           1450
44 *TAPE=1.                                1460
    CALL EDIT                               1470
    II=II+1                                1480
    NTEDT=1                                1490
45 TIME=TIME+DTNH                         1500
    DTN=DTN+DTNH                         1510
    N=N+1                                 1520
    IF (DTNH) 46,46,2                   1530
46 PAUSE2:                                1540
    GO TO 2                                1550
    END

```

GENERATOR SUBROUTINE FOR THE PUFF HYDRO CODE

SUBROUTINE GENRAT

```

COMMON CS(500),CUSP1(6),CUSPA(6),CUSPC(6),CUSPU(6),CUSPG(6),
1CUSPS(6),DISCPT(12),E(500),ECSTC(6),EQSTD(6),EQSTC(6),EQSTG(6)
26),EQSTH(6),EQSTN(6),EQSTS(6),JBND(6),JEDIT(10),JCP(10),MATL(6),V(6),
3Z(20),P(500),PMIN(6),Q(500),PHO(6),RZ(20),TEDIT(25),U(100),V(100),
4X(500),ZM(500)
COMMON CKP,DTN,DTNH,JCK,JCYCS,JFIN,JFIN2,JPMAX,JRZL,JUTAP,JXXS,JZP,
IUL,LINE,N,NJEDIT,NMTRLS,NPRIN,NR2,NTAPE,NTEDT,PMAX,TIME,TM,JZPUL,
2WTAPE,ZPUL

FORMAT(10A8)                                1640
FORMAT(8I10)                                 1650
FORMAT(8E10.3)                               1660
FORMAT(4SH EROR--INPUT CARDS ARE NOT PROPERLY PREPARED) 1670
FORMAT(2EH1INPUT PARAMETERS FOR - --/1H01CAR) 1680
FORMAT(4SH *** THIS PROBLEM WAS RUN ON P-PUFF/1604 *** ) 1690
FORMAT(1HC5X,4HNRZC4X,6HNMTLS6X,4HURZLEX,5HJZPULSX,5HNPINEX,
1SHFACEEX,5HZERO5X,5HJFIN2/5I10,2E10,3,I10) 1700
FORMAT(//17H ZONING CONSTANTS//)             1710
FORMAT(3X,6H RATIOE10.3,BH TO ZONE) 1720
FORMAT(1HC5X,4HJFIN5X,5HJCYCS5X,5HNTAPE7X,3HCKPRX,2HT06
1X,4HTIME/4I10,3E10.3) 1730
FORMAT(25HOMATERIAL PROPERTIES FOR A6.5X,4HRHO=E10.3,EX,7HFRC J=
115.2X,5HT0 J=15) 1740
FORMAT(1HC9X,5HEGSTC1CX,5HEGSTD1CX,5HEGSTE1CX,5HEGSTG1CX,5HEGSTH1
10X,5HEGSTS1CX,5HEGSTN1CX,4HPMIN/3E15.5) 1750
FORMAT(1HC9X,5HCUSP110X,5HCUSPA10X,5HCUSPC10X,5HCUSPD10X,5HCUSPS
11CX,5HCUSPS/6E15.5) 1760
FORMAT(1H1,10A8/5H0 J 6X,1HXRX,8HVELOCITYSX,9HZONE MASS//) 1770
FORMAT(1H 13,3E14.5) 1780
FORMAT(1H1) 1790
FORMAT(1HC1CX,14HTHE TEDIT'S ARE/10E10.3/) 1800
FORMAT(1HC1CX,14HTHE JEDIT'S ARE/10I10) 1810
FORMAT(21H MATERIAL THICKNESS =E10.3) 1820

```

READ DATA

```

READ 1,(DISCPT(I),I=1,10) 1830
READ 2,NRZC,NMTRLS,JRZL,JZPUL,NPRIN,NTAPE,NJEDIT,NTEDT 1840
IF(NTEDT) 21,21,20 1850
READ 3,(TEDIT(I),I=1,NTEDT) 1860
IF(NJEDIT) 23,23,22 1870
READ 2,(JEDIT(I),I=1,NJEDIT) 1880
ZPUL=JZPUL 1890
NMTRLS=NMTLS-1 1900
READ 3,UFACE,UZERO,UFIN2 1910
JFIN2=UFIN2 1920
IF(NMT) 25,25,24 1930
READ 2,(JBND(M),M=1,NMT) 1940
READ 2,JFIN,(NZ(L),L=1,NRZC) 1950
READ 3,DX,TIME,(RZ(M),M=1,NRZC) 1960
DX=DX/RZ(1) 1970
DO 26 M=1,NMTRLS 1980

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```

READ 1, MATL(M)
READ 3, RHO(M), EQSTC(M), EQSTD(M), EQSTE(M), EQSTG(M), EQSTH(M), F1, F2, F3, F4
1, FMIN(M)
READ 3, CUSP1(M), CUSPA(M), CUSPC(M), CUSPD(M), CUSPG(M), CUSPS(M)
26 EQSTNM(M)=EQSTC(M)/EQSTG(M)/(EQSTE(M)*RHO(M))
READ 3, CKP, TS
READ 2, JCYCS, NTEST
IF (NTEST=30) 27, 28, 27
27 PRINT 4
STOP
28 CONTINUE
IF (NJEDIT) 31, 31, 29
29 DO 30 I=1, NJEDIT
30 JORG(I)=JEDIT(I)
31 JK=0
JXX0=0
NP7=-50
C
C          SET PLATE VELOCITY
C
DO 32 J=1, JFIN2
U(J)=UZERO
CONTINUE
32 U(JFIN2)=UZERO*(1.+UFACE)/2.
U(JFIN2+1)=UZERO*UFACE
U(JFIN2+2)=U(JFIN2+1)/2.0
C
C          COMPUTE DX USING ZONEING CONSTANTS
C
LZ=1
DO 33 J=1, JFIN
IF (J=1-N7(LZ)) 34, 33, 34
33 LZ=LZ+1
34 DX=DX+N7(LZ)
35 X(J+1)=X(J)+DX
C
C          SET UP ZONING FOR HYDRO
C
M=1
DO 37 J=2, JFIN
V(J)=1./RHO(M)
ZM(J)=(X(J)-X(J-1))/V(J)
IF (J=JEND(M)) 37, 36, 37
36 V=N+1
37 CONTINUE
C
C          START INPUT EDIT
C
PRINT 5
PRINT 1, DISCPT(K), K=1, 10
PRINT 6
PRINT 7, NRZC, NTRLC, JPZL, JZPUL, NPPIN, UFACE, UZERO, JFIN2
PRINT 8
PRINT 9, NZ(1), NZ(1)+I=1, NRZC
PRINT 10, JFIN, JCYCS, NTEST, NTAPE, CKP, TS, TIME
IF (NJEDIT) 11, 39, 39
39 PRINT 12, JEDIT(I), I=1, NJEDIT

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```

47 IF (JF < 1) 40,41,42
48 PRINT 17,JF,DISCPT(1),I=1,NTELT
49 JF1=1
50 PRINT 16
51 DC 47 K=1,NMTRLS
52 IF (JF-NP(M)) 42,42,43
53 JF2=JF1N
54 GO TO 44
55 JF2=JFND(M)
56 THKNS=EX(JF2)-X(JF1)
57 PRINT 11,MATL(M),RHO(M),JF1,JF2
58 PRINT 19,THKNS
59 PRINT 12,EGSTC(M),EGSTR(M),EGSTH(M),EGSTC(M),EGSTR(M),EGSTH(M),EGSTC(M),EGSTR(M)
60 ITN(M),PMIN(M)
61 IF (CUPRAT(M)) 46,46,45
62 PRINT 13,CUP1(M),CUPRA(M),CUPSC(M),CUPSH(M),CUPRG(M),CUPRS(M)
63 JF1=JF2
64 CONTINUE
65
66          START VELOCITY EDIT
67
68 PRINT 14,(DISCPT(1),I=1,10)
69 JSOX=JF1N2+3
70 DC 49 J=1,JSOX
71 PRINT 15,J,X(J),U(J),ZM(J)
72 IF (XMODF(J,50)) 49,48,42
73 PRINT 14,(DISCPT(1),I=1,10)
74 CONTINUE
75 PRINT 16
76 RETURN
77 END

```

```

780
790
7960
7970
7980
7990
8000
8010
8020
8030
8040
8050
8060
8070
8080
8090
8100
8110
8120
8130
8140
8150
8160
8170
8180
8190
8200
8210
8220
8230
8240
8250
8260
8270
8280
8290
8300
8310
8320
8330
8340

```

ROUTINE SUBROUTINE FOR THE E-1 FILE HYDRO

IN ROUTINE REZONE

COMMON C(500),CUSPL(6),CUTPA(6),CUTPC(6),CUTPD(6),CUSPG(6),
100TPC(6),V0ISCP(12),E(500),EGTC(6),EGTE(6),EQSTG(6),
261,EGTH(6),EGTN(6),EGTS(6),JPN(6),JNET(10),JORG(10),NATE(6),
321,1,P(500),PMIN(6),Q(500),RHO(6),RZ(20),TEdit(25),U(500),V(500),
4X(500),TM(500)
COMMON CXP,DTN,DTNH,JCK,JCYC,JFIN,JFIN2,JPMAX,JRZL,JSTAR,JXXC,JZP
TUL,LINE,N,NJEDIT,NNTAL,NPRINT,NRZ,NTAPE,NTEDT,PMAX,TIME,TH,ZERO,
ZTAPE,ZPUL

FORMAT (F10.3,2I10)

REZONE AHEAD OF MAIN PRESSURE PULSE

SCRNCH=0.
WTAPE=1.
IF (JPMAX-JZPUL-JRZL-10) 85,85,
JV=1
M=1
DO 6 JV=1,JSTAR
IF (J-JEND(M)) 4,3,4
M=M+1
IF (RHO(M)*V(J+1)-1.2) 7,5,5
JV=J
CONTINUE
IF (ZPUL) 46,46,7
J=MJMAX+3
XJPMAX=X(JPMAX)
EMVPL=0.
EMVPL=EMVPL+U(J)*.5*(Z(J)+Z(J+1)+Z(J+2))
IF (U(J+1)) 12,12,10
IF (U(J-1)) 12,12,11
J=MJ-1
GO TO 9
JM=JPMAX+4
EMVPR=0.
EMVPR=EMVPR+U(J)*2.*((Z(J)+Z(J+1))
IF (J=M-JSTAR) 14,14,15
JM=JM+1
GO TO 13
EMVPP=EMVPL+EMVPR
DTDP=EMVPP/PMAX
DTDP=X=2.*DTDP*C(JMAX)/ZPUL
J=JPMAX
J=J+1
IF (J+1-JFIN) 17,46,46
17 IF (X(J)-X(J-1)-RZDX) 18,18,19
18 IF (J-JPMAX-20) 16,46,46
19 IF (J-JXXC) 46,46,27
CALL EDIT
SCRNCH=1.
JFIN0=JFIN
JXXC=J
DO 22 M=1,NMTRLS

```

21 IF (J=1-J-N (ME)) 23,21,22          3610
    J=J+1
22 CONTINUE
    NCK=NUTRLS
23 ME=MCK
24 IF (JCK) 25,25,26          3670
25 RZR=.5*(X(J-1)+X(J))-X(J-2))/((X(J)-X(J-2))
    EL=E(J-1)+RZR*(E(J)-E(J-1))          3680
    VL=V(J-1)+RZR*(V(J)-V(J-1))
    IF (J-JNND(ME)) 26,27,26          3690
26 RZR=(X(J+1)-.5*(X(J)+X(J-1)))/((X(J+1)-X(J-1))
    ER=E(J)+RZR*(E(J)-E(J-1))          3700
    VR=V(J)+RZR*(V(J)-V(J-1))          3710
    IF (JCK) 28,29,28          3720
27 RZR=(.5*(X(J)-X(J-1)))/((X(J)-X(J-2))          3730
    ER=E(J)+RZR*(E(J)-E(J-1))          3740
    VR=V(J)+RZR*(V(J)-V(J-1))          3750
    GO TO 29          3760
28 RZR=(.5*(X(J)-X(J-1)))/((X(J+1)-X(J-1))          3770
    EL=E(J)+RZR*(E(J)-E(J+1))          3780
    VL=V(J)+RZR*(V(J)-V(J+1))          3790
29 XR=X(J)
    XL=.5*(X(J)+X(J-1))          3800
    ZMR=(XR-XL)/VP          3810
    ZML=(XR-XL)/VL          3820
    UR=U(J)
    UL=((ZM(J)-ZML)*U(J-1)+(ZM(J)-ZMR)*U(J))/(ZML+ZMR)
    DEN=1./VL          3830
    CALL EGST (EL,DEN,PL,ME)
    DEN=1./VR          3840
    CALL EGST (ER,DEN,PR,ME)
    QL=Q(J)
    QR=Q(J)
    CSL=CS(J)
    CSR=CS(J)
    JDO=J
    JI=ME
    DC 31 NME=JDO,JFIN
    IF (NME-JBND(JI)) 31,30,31          3850
30 JNND(JI)=NME+1          3860
    JI=JI+1          3870
31 CONTINUE
    JXX=J          3880
    J=JFIN          3890
32 X(J+1)=X(J)          3900
    U(J+1)=U(J)          3910
    ZM(J+1)=ZM(J)          3920
    V(J+1)=V(J)          3930
    E(J+1)=E(J)          3940
    P(J+1)=P(J)          3950
    Q(J+1)=Q(J)          3960
    CS(J+1)=CS(J)          3970
    J=J-1          3980
    IF (J-JXX) 33,33,32          3990
33 X(J+1)=XR          4000
    X(J)=XL          4010
    U(J+1)=UR          4020

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```

U(J)=UL
ZM(J+1)=ZMR
ZM(J)=ZML
V(J+1)=VR
V(J)=VL
E(J+1)=ER
E(J)=EL
P(J+1)=PR
P(J)=PL
Q(J+1)=QR
Q(J)=QL
CS(J+1)=CSR
CS(J)=CSL
IF(NJEDIT) 37,37,34
30 36 11=NJEDIT
IF(J=JEDIT(1)) 35,35,36
35 JEDIT(1)=JEDIT(1)+1
CONTINUE
37 IF(J=JSTAR) 38,38,39
38 JSTAR=JSTAR+1
39 JFIN=JF(N+1)
40 IF (X(J)-X(J-1)=RZDX) 40,24,24
41 IF (J=JXX0-20) 41,45,45
42 J=J+2
43 IF (J=JFIN) 42,45,45
44 IF (J=1-JEND(MF)) 43,44,43
45 JCK=0
46 GO TO 26
47 M=M+1
48 JCK=1
49 GO TO 26
50 JRZ=JFIN-JFIN
51 PRINT 1,TIME,N,JRZ,JSTAR
52
53 REZONE BEHIND MAIN PRESSURE PULSE
54
55 IF (JRZL) 85,85,47
56 IF (N-NRZ=100) 85,85,48
57 JRZV=1
58 MZ=1
59 JFINO=JFIN
60 JFINS=JFIN+1
61 M=MRZ
62 KRZ=0
63 J=JPMAX
64 J=J-1
65 IF (P(J)/PMAX=.2) 50,50,49
66 JPLC=J
67 IF (JPLC-JV-JRZL) 51,51,58
68 IF (JPMAX-JPLC-JZPUL) 52,52,53
69 IF (KRZ) 85,85,84
70 J=JPLC+1
71 DO 54 MM=1,NMTRLS
72 IF (JPLC+1-JEND(MM)) 53,53,54
73 CONTINUE
74 MM=NMTRLS
75 M=MM

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```

DO 56 MM=1,NMTRLS          4760
IF (JPMAX-JRND(MM)) 57,57,56
56 CONTINUE                  4770
MM=NMTRLS                  4780
57 RZR=RZDX*.5*V(JPMAX)*RHO(NM) 4790
KRZ=-1                      4800
GO TO 61                     4810
KRZ=1                        4820
58 DO 59 MM=1,NMTRLS          4830
IF (JV+1-JBND(MM)) 60,60,59
59 CONTINUE                  4840
MM=NMTRLS                  4850
60 M=MM                      4860
RZR=(X(JPLC)-X(JV))/FLOATE(JRZL)
JV=JV+1                      4870
61 IF (SCRNCH) 62,62,63
62 CALL EDIT                  4880
SCRNCH=1.
63 IF (X(J+1)-X(J)-RZR) 64,79,79
64 IF (J+1-JBND(M)) 65,79,65
65 IF (NJEDIT) 68,68,66
66 DO 67 II=1,NJEDIT          4890
IF (J+1-JEDIT(II)) 67,79,67
67 CONTINUE                  4900
68 ZMINV=1./(ZM(J+1)+ZM(J+2))
V(J+1)=(V(J+1)*ZM(J+1)+V(J+2)*ZM(J+2))*ZMINV
E(J+1)=(E(J+1)*ZM(J+1)+E(J+2)*ZM(J+2))*ZMINV
DEN=1./V(J+1)
CALL EGST (E(J+1),CEN,P(J+1),M)
UA=(ZM(J)*U(J)+ZM(J+1)*(U(J)+U(J+1)))/(ZM(J)+2.*ZM(J+1))
ZMC=ZM(J+3)+2.*ZM(J+2)
IF (ZMC) 69,70,69
69 UB=(ZM(J+3)*U(J+2)+ZM(J+2)*(U(J+2)+U(J+1)))/ZMC
GO TO 71
70 UB=C.
71 ZM(J+1)=ZM(J+1)+ZM(J+2)
Q(J+1)=(Q(J+1)+Q(J+2))/2.0
CS(J+1)=(CS(J+1)+CS(J+2))/2.0
U(J)=UA
U(J+1)=UR
X(J+1)=X(J+2)
JX=J+2
DO 72 JC=JX,JFINS          5000
X(JC)=X(JC+1)
U(JC)=U(JC+1)
ZM(JC)=ZM(JC+1)
V(JC)=V(JC+1)
E(JC)=E(JC+1)
P(JC)=P(JC+1)
Q(JC)=Q(JC+1)
CS(JC)=CS(JC+1)
72 CONTINUE                  5010
JFIN=JFIN-1
IF (NJEDIT) 76,76,73
73 DO 75 II=1,NJEDIT          5020
IF (J-JEDIT(II)) 74,74,75
74 JEDIT(II)=JEDIT(II)-1      5030

```

75	CONTINUE	5430
76	JPMAX=JPMAX-1	5440
	JSTAR=JSTAR-1	5450
	JPLC=JPLC-1	5460
	JXXO=JXXO-1	5470
	DO 7H M1=1,NMPLS	5480
	IF (JFND(M1)=J+2) 7B,77,77	5490
	JFND(M1)=JFND(M1)-1	5400
78	CONTINUE	5410
79	END COLAPS	5420
80	IF (K97) 81,85,80	5430
81	IF (J=JPLC) 82,81,81	5440
82	IF (J+4=JPMAX) 82,84,84	5450
83	J=J+1	5460
	IF (J=JFND(M1)) 63,83,63	5470
84	M=M+1	5480
	DO 80 63	5490
85	JF7=JF1NO-JF1K	5500
	NRZ=N	5510
	PRINT 1,TIME+N,JRZ,JSTAR	5520
	CONTINUE	5530
86	IF (SCPNCH) 87,87,86	5540
87	CALL EDIT	5550
	RETURN	5560
	END	5570

```

C EDIT SUBROUTINE FOR THE PUFF HYDRODYNAMIC CODE
C SUBROUTINE EDIT
C
COMMON CS(500),CUSP1(6),CUSPA(6),CUSPC(6),CUSPD(6),CUSPG(6),
1CUUPS(6),DISCPT(12),E(500),EQSTC(6),EQSTD(6),EQSTE(6),EQSTG(
26),EQSTH(6),EQSTN(6),EQSTS(6),JBND(6),JEDIT(10),JORG(10),MATL(6),N
37(20),P(500),PMIN(6),Q(500),PHO(6),RZ(20),TEDIT(25),U(500),V(500),
4X(500),ZM(500)
COMMON CKP,CTN,DTNH,JCK,JCYCLE,JFIN,JFIN2,JPMAX,JRZL,JSTAR,JXX0,JZF
5LL,LINE,N,NJEDIT,NMTRLS,NPRIN,NRZ,NTAPE,NTEDT,PMAX,TIME,TS,UZERO,
6NTAPE,ZPUL
C
FORMAT(1H6,XSHCYCLE8X,4HTIME8X,4HDTNH7X,5HJSTAR7X,5HJPMAX8X,4HFMA
1X6X,6HXJPMAX5X,7HMVPULSE6X,6HMVFREC4X,8HMOMENTUM/2X,110,2E12.4,
22112,5E12.4/8X4HUTPP6X,6HOTPULS6X,6HETOTAL6X,6HE(VNEG6X,6HEMVPOS5X
3,7HL-ROUND4X,8HX(JBND1)4X,8HX(JBND2)5X,7HR-BOUNDBX,4HUFIN/9E12.4,
4112)
FORMAT(1H1)
C BINARY DATA STORAGE
XJPNT=X(JPMAX)
IF (NTAPE) 3,7,3
JSTAR=JSTAR+1
WRITE TAPE 6,N,TIME,(DISCPT(I),I=1,10),JSTAR,JFIN,JPMAX,JSTAR
IF (EOF,6) 5,4
WRITE TAPE 6,(J,X(J),U(J),P(J),Q(J),E(J),V(J),CS(J),J=1,JSTAR)
IF (EOF,6) 5,7
PRINT 6,N
FORMAT (16H NEW 06 AT CYCLE10)
END FILE 6
REWIND 6
PAUSE12345
GO TO 3
C
C MOMENTUM AND ENERGY CALCULATION
C
EMVNEG=0.
EMVPOS=0.
FSUM=0.
EKSUM=0.
JSTAR=JSTAR+1
DO 11 J=2,JSTAR
EMV=2M(J)*(U(J)+U(J-1))/2.
IF (EMV) 8,9,9
EMVNEG=EMVNEG+EMV
GO TO 10
EMVPOS=EMVPOS+EMV
CONTINUE
FSUM=FSUM+E(J)*ZM(J)/4.186E7
EKSUM=EKSUM+ZM(J)*(U(J)+U(J-1))**2/4.186E7/9.
CONTINUE
ETOTAL=FSUM+EKSUM
JMF=JPMAX+3
EMVPL=0.
EMVPL=EMVPL+U(JM)*.5*(ZM(JM+1)+ZM(JM))
IF (JM-JPMAX) 13,14,14
IF (U(JM-1)) 16,16,14
IF (U(JM-1)) 16,16,15

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15 JM=JM-1
16 GO TO 12
17 JM=JPMAX+4
EMVPR=0.
18 EMVPR=EMVPR+U(JM)/2.*((ZM(JM)+ZM(JM+1))
19 IF (JM-JFIN) 18,18,19
20 JM=JM+1
21 GO TO 17
22 EMVPR=EMVPL+EMVPR
23 DTPP=EMVPR/PMAX
24 DTPULS=EMVPL/PMAX
25
26 PRINT OUTPUT VARIABLES
27
28 JBNDC1=JRNDC(1)
29 JBNDC2=JRNDC(2)
30 PRINT 1,N,TIME,DTNH,JSTAR,JPMAX,PMAX,XJPMAX,EMVPL,EMVPR,EMVPP,DTPP
31 DTPULS,TOTAL,EMVNEG,EMVPOS,X(1),X(JBNDC1),X(JBNDC2),X(JFIN),JFIN
32 LINE=LINE+5
33 IF (XMODE(LINE,SC)) 21,20,21
34 PRINT ?
35 RETURN
36 END

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C EQUATION OF STATE SUBROUTINE FOR THE PUFF HYDRODYNAMIC CODE          6410
C SUBROUTINE EOST (E1,D,P1,M)                                         6420
C
C COMMON CS(500),CUSP1(6),CUSPA(6),CUSPC(6),CUSPD(6),CUSPG(6),        6430
C ICUSPS(6),DISCPT(12),E(500),EQSTC(6),EQSTD(6),EQSTE(6),EOSG(        6440
C 26),EOSTH(6),EQSTN(6),EQSTS(6),JSND(6),JEDIT(10),JORG(10),MATL(6),    6450
C 32(20),P(500),PMIN(6),Q(500),RHO(6),R7(20),TEDIT(25),U(500),V(500),  6460
C 4X(500),ZN(500)                                                 6470
C COMMON CKE,DTN,DTNH,JCK,JCYCS,JFIN,JFIN2,JPMAX,JRZL,JSTAR,JXX0,JZP
C IUL,LINC,N,NJEDIT,NMTPLS,NPRIN,NRZ,NTAPE,NTEDT,PMAX,TIME,TS,UZEPO,
C 2VTAPE,ZPIL
C
C   ENU=D/RHO(M)
C   EMU=ENU-1.
C   V1=D40(M)/D
C   IF (EMU) 1,5,6
C
C     VAPOR EQUATION
C
C   ENU2=EQSTN(M)*(1.-V1)*V1
C   IF (ENU2+1.,) 3,3,2
C   T1=EQSTE(M)*(1.-EXP(-ENU2))
C   GO TO 4
C   T1=EQSTE(M)
C   TS2=ENU*(EOSTH(M)+(EQSTG(M)-EOSTH(M))*SQRTE(ENU))
C   PI=MAX(PMIN(M)+(E1-TS1)*TS2*RHO(M))
C   GO TO 9
C
C     TWO-WAVE SOLID EQUATION
C
C   IF (CUSPA(M)) 8,8,6
C   ARG=EMU-CUSPA(M)
C   IF (ARG) 8,8,7
C   TS2=((CUSPS(M)*ARG+CUSPD(M))*ARG+CUSPC(M))*ARG
C   PI=CUPP1(M)+TS2+E1*CUSPG(M)*D
C   GO TO 9
C
C     ONE-WAVE SOLID EQUATION
C
C   TS2=(EQSTS(M)*EMU+EQSTD(M))*EMU+EQSTC(M)*EMU
C   PI=TS2+E1*EQSTC(M)*D
C   RETURN
C   END

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APPENDIX III

TEST PROBLEM 1

(PUFF)

10	MATL(1) MATL 1					
9	DX 1.3	TIME 1.12	RZ(1) 1.02	RZ(2) 1	RZ(3) 103	
8	JFIN 282	NZ(1) 82	NZ(2) 82	NZ(3) 281		
7	JBND(1) 82					
6	SPUR 3-8	T(1) 0	EE(1) 0			
5	NØE(1) 11	NØE(2) 7				

4	ANGLE 0.						
3	NBB 1	NRZC 3	NMTRLS 2	JRZL 100	JZPUL 40	NPRIN 25	TAPE 25
2	DISCPT(I), I=1,10 *** TEST PROBLEM NØ 1 *** TWO MATERIAL *** ARBITRARY SPECTRUM						
1	TABLE DECK FOR PROBLEM 1						
	NHNU 109	NTEDT 0	NJEDIT 0	LØZHIZ 1			

72	EDGE(2,3) 4.132+1	AA(2,4) 6.951+2	B(2,4) -1.984	EDGE(2,4) 4.958+1	AA(2,5) 1.723+2	B(2,5) -1.562	EDGE(2,5) 6.198+1	AA(2,6) 2.793+1
21	AA(2,1) 2.267+2	B(2,1) -2.606	EDGE(2,1) 1.559	AA(2,2) 1.535+4	B(2,2) -2.78	EDGE(2,2) 3.099+1	AA(2,3) 3.161+3	B(2,3) -2.323
20	CUSP1(2) 0.	CUSPA(2) 0.	CUSPC(2) 0.	CUSP5(2) 0.	CUSPG(2) 0.	CUSPS(2) 0.		
19	RH0(2) 2.699	EQSTC(2) 8.5+11	EQSTD(2) -1.232+12	EQSTE(2) 1.22+11	EQSTG(2) 2.04	EQSTM(2) .25	EQSTS(2) 0.	PMIN(2) -6.+9
18	MATL(2) MATL 2							
	EDGE(1,1) 1.50+2							

16	AA(1,9) 1.7121	B(1,9) -5.8565-1	EDGE(1,9) 4.9584+1	AA(1,10) 7A640-1	B(1,10) -3.5298-1	EDGE(1,10) 6.198+1	AA(1,11) 5.8627-1	B(1,11) -2.9836-1
15	B(1,6) -1.5975	EDGE(1,6) 2.4792+1	AA(1,7) 1.4021+1	B(1,7) -1.1633	EDGE(1,7) 3.099+1	AA(1,8) 3.3035	B(1,8) -7.4228-1	EDGE(1,8) 4.132+1
14	EDGE(1,3) 1.2396+1	AA(1,4) 2.259+2	B(1,4) -2.0539	EDGE(1,4) 1.5495+1	AA(1,5) 2.251+2	B(1,5) -2.0539	EDGE(1,5) 2.066+1	AA(1,6) 5.8508+1
13	AA(1,1) 6.565+2	B(1,1) -2.8569	EDGE(1,1) 1.870-1	AA(1,2) 6.612+2	B(1,2) -2.8571	EDGE(1,2) 2.840-1	AA(1,3) 1.878+3	B(1,3) -2.8568
2	CUSP1(1) 0.	CUSPA(1) 0.	CUSPC(1) 0.	CUSPD(1) 0.	CUSPG(1) 0.	CUSPS(1) 0.		
	RH0(1) 2.2	EQSTC(1) 2.513+11	EQSTD(1) 1.668+11	EQSTE(1) 7.59+10	EQSTG(1) .75	EQSTM(1) .25	EQSTS(1) 1.748+13	PMIN(1) -1.+9

25	JCYCS 250	NTEST 30			
24	CKP 1.0	TS 2.-6			
23	B(2,6) -1.121	EDGE(2,6) 8.264+1	AA(2,7) 2.581	B(2,7) -5.876-1	EDGE(2,7) 1.50+2

TABLE DECK FOR TEST PROBLEM 1

2E15.7 FORM.F

<u>TBL(I)</u>	<u>L(I)</u>	<u>TBL CAP #</u>
0.5972897E 00	0.	1
0.7712318E 00	0.	2
0.8991189E 00	0.	3
0.1004823E 01	0.	4
0.1097018E 01	0.	5
0.1179999E 01	0.	6
0.1256234E 01	0.	7
0.1327283E 01	0.	8
0.1394228E 01	0.	9
0.1457829E 01	0.	10
0.1518656E 01	0.	11
0.1577137E 01	0.	12
0.1633631E 01	0.	13
0.1688417E 01	0.	14
0.1741701E 01	0.	15
0.1793693E 01	0.	16
0.1844536E 01	0.	17
0.1894372E 01	0.5026790E-30	18
0.1943309E 01	0.9455565E-28	19
0.1991455E 01	0.10164E7E-25	20
0.2038900E 01	0.6780110E-24	21
0.2085728E 01	0.3002525E-22	22
0.2132004E 01	0.9325856E-21	23
0.2177796E 01	0.2127423E-19	24
0.2223151E 01	0.3701496E-18	25
0.2268135E 01	0.5078059E-17	26
0.2312798E 01	0.5645669E-16	27
0.2357167E 01	0.5202916E-15	28
0.2401296E 01	0.4058228E-14	29
0.2445216E 01	0.2725063E-13	30
0.2488976E 01	0.1600093E-12	31
0.2532594E 01	0.8319149E-12	32
0.2576116E 01	0.3876429E-11	33
0.2619573E 01	0.1635183E-10	34
0.2662981E 01	0.6297824E-10	35
0.2706380E 01	0.2233014E-09	36
0.2749789E 01	0.7338907E-09	37
0.2793255E 01	0.2250884E-08	38
0.2836786E 01	0.6475984E-08	39
0.2880413E 01	0.1756749E-07	40

<u>TBL(I)</u>	<u>EI(I)</u>	<u>TEL CALL #</u>
0.2924164E 01	0.4512999E-07	41
0.2968066E 01	0.1103210E-06	42
0.3012138E 01	0.2573599E-06	43
0.3056410E 01	0.5750408E-06	44
0.3100911E 01	0.1234469E-05	45
0.3145668E 01	0.2553269E-05	46
0.3190700E 01	0.5100153E-05	47
0.3236046E 01	0.9863331E-05	48
0.3281714E 01	0.1850221E-04	49
0.3327763E 01	0.3374433E-04	50
0.3374200E 01	0.5992323E-04	51
0.3421056E 01	0.1037839E-03	52
0.3468368E 01	0.1755874E-03	53
0.3516174E 01	0.2908129E-03	54
0.3564503E 01	0.4711179E-03	55
0.3613382E 01	0.7489089E-03	56
0.3662859E 01	0.1168785E-02	57
0.3712972E 01	0.1792640E-02	58
0.3763772E 01	0.2704874E-02	59
0.3815276E 01	0.4017908E-02	60
0.3867541E 01	0.5881003E-02	61
0.3920633E 01	0.8489057E-02	62
0.3974593E 01	0.1209454E-01	63
0.4029434E 01	0.1701714E-01	64
0.4085395E 01	0.2366080E-01	65
0.4142310E 01	0.3253191E-01	66
0.4200384E 01	0.4425427E-01	67
0.4259677E 01	0.5959707E-01	68
0.4320261E 01	0.7948911E-01	69
0.4382229E 01	0.1050552E-00	70
0.4445692E 01	0.1376467E-00	71
0.4510757E 01	0.1788674E-00	72
0.4577551E 01	0.2308213E-00	73
0.4646193E 01	0.2951281E-00	74
0.4716850E 01	0.3750174E-00	75
0.4789699E 01	0.4733590E-00	76
0.4864916E 01	0.5936806E-00	77
0.4942714E 01	0.7400929E-00	78
0.5023361E 01	0.9173987E-00	79
0.5107114E 01	0.11131043E-01	80
0.5194313E 01	0.1387413E-01	81
0.5285303E 01	0.1693737E-01	82
0.5380537E 01	0.2058509E-01	83
0.5480544E 01	0.2491980E-01	84
0.5585897E 01	0.3004178E-01	85

<u>TBL(I)</u>	<u>EL(I)</u>	<u>TBL C.M. #</u>
0.5697338E 01	0.3609566E 01	86
0.5815793E 01	0.4323557E 01	87
0.5942340E 01	0.5164528E 01	88
0.6078354E 01	0.6154630E 01	89
0.6225589E 01	0.7320720E 01	90
0.6380413E 01	0.8696669E 01	91
0.6563949E 01	0.1032499E 02	92
0.6762600E 01	0.1226171E 02	93
0.6988700E 01	0.1458224E 02	94
0.7252136E 01	0.1739563E 02	95
0.7559328E 01	0.2086893E 02	96
0.7970381E 01	0.2528069E 02	97
0.8523455E 01	0.3119787E 02	98
0.9445122E 01	0.4017112E 02	99
0.9582477E 01	0.4139209E 01	100
0.9735226E 01	0.4271261E 01	101
0.9907640E 01	0.4415586E 01	102
0.1010589E 02	0.4575365E 01	103
0.1033309E 02	0.4690531E 01	104
0.1062301E 02	0.4836915E 01	105
0.1098729E 02	0.5014182E 01	106
0.1149372E 02	0.5244321E 01	107
0.1237449E 02	0.5593458E 01	108
0.1425603E 02	0.6181078E 01	109

INPUT PARAMETERS FOR -

*** TEST PROBLEM NO. 1 *** TWO MATERIAL *** ARBITRARY SPECTRUM
*** THIS PROBLEM WAS RUN ON PUFF/1604. ***

TABLE VALUES

5.973E-01	7.712E-01	8.991E-01	1.1005E	0.00	1.397E	0.00	1.180E	0.00	1.256E	0.00	1.327E	0.00	1.394E	0.00	1.458E	0.00			
1.519E	0.00	1.577E	0.00	1.634E	0.00	1.688E	0.00	1.742E	0.00	1.794E	0.00	1.845E	0.00	1.894E	0.00	1.943E	0.00	1.991E	0.00
2.039E	0.00	2.086E	0.00	2.132E	0.00	2.173E	0.00	2.223E	0.00	2.268E	0.00	2.313E	0.00	2.357E	0.00	2.401E	0.00	2.445E	0.00
2.489E	0.00	2.533E	0.00	2.576E	0.00	2.620E	0.00	2.663E	0.00	2.706E	0.00	2.750E	0.00	2.793E	0.00	2.837E	0.00	2.880E	0.00
2.924E	0.00	2.968E	0.00	3.012E	0.00	3.056E	0.00	3.101E	0.00	3.146E	0.00	3.191E	0.00	3.236E	0.00	3.282E	0.00	3.328E	0.00
3.374E	0.00	3.421E	0.00	3.468E	0.00	3.516E	0.00	3.565E	0.00	3.613E	0.00	3.663E	0.00	3.713E	0.00	3.764E	0.00	3.815E	0.00
3.868E	0.00	3.921E	0.00	3.975E	0.00	4.029E	0.00	4.085E	0.00	4.142E	0.00	4.200E	0.00	4.260E	0.00	4.320E	0.00	4.382E	0.00
4.446E	0.00	4.511E	0.00	4.578E	0.00	4.646E	0.00	4.717E	0.00	4.790E	0.00	4.865E	0.00	4.943E	0.00	5.024E	0.00	5.107E	0.00
5.194E	0.00	5.285E	0.00	5.381E	0.00	5.481E	0.00	5.586E	0.00	5.697E	0.00	5.816E	0.00	5.942E	0.00	6.078E	0.00	6.226E	0.00
6.388E	0.00	6.564E	0.00	6.763E	0.00	6.989E	0.00	7.252E	0.00	7.569E	0.00	7.970E	0.00	8.523E	0.00	9.445E	0.00	9.582E	0.00
9.735E	0.00	9.908E	0.00	1.011E	0.01	1.034E	0.01	1.062E	0.01	1.099E	0.01	1.150E	0.01	1.238E	0.01	1.425E	0.01		

EITOT = 2.7242272E 02

L0PHIL = 1

ZONING CONSTANTS

RATIO 1.020E 00	TO ZONE 51
RATIO 1.000E-01	TO ZONE 62
RATIO 1.030E 00	TO ZONE 281

BLACK BODY TEMPERATURE AND ASSOCIATED ENERGY
TEMPERATURE ENERGY 0

JFIN 282	JCYCS 250	NTEST 30	NTAPt 25	CKP 1.000E 00	T\$ 2.000E-06	TIME 1.000E-12	SOUR 3.000E-08
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MATERIAL PROPERTIES FOR MATTL 1
MATERIAL THICKNESS = 1.986E-01

RHO= 2.200E 00 FROM J= 1 TO J= 82

EQSTC	EQSTD	EQSTC	EQSTG	EQSTH	EQSTS	EQSTM	PMIN
2.51300E 11	1.66800E 11	7.59000E 10	7.50000E-01	2.50000E-01	1.74000E 13	2.00663E 00	-1.00030E 09

NOE = 11 AA B EDGE

6.56500E 02		-2.05690E 00		1.87000E-01			
6.61200E 02		-2.05710E 00		2.04000E-01			
1.87800E 03		-2.05680E 00		1.23960E 01			
2.25900E 02		-2.05390E 00		1.54950E 01			
2.25100E 02		-2.05340E 00		2.06600E 01			
5.65080E 01		-1.59750E 00		2.47920E 01			
1.40210E 01		-1.16330E 00		3.09900E 01			
3.30350E 00		-7.42280E-01		4.13200E 01			
1.71210E 00		-5.65650E-01		4.95640E 01			
7.46480E-01		-3.52980E-01		6.19800E 01			
5.86270E-01		-2.99360E-01		1.50000E 02			

MATERIAL PROPERTIES FOR MATTL 2
MATERIAL THICKNESS = 5.986E 00

RHO= 2.699E 00 FROM J= 82 TO J= 282

EQSTC	EQSTD	EQSTC	EQSTG	EQSTH	EQSTS	EQSTM	PMIN
8.50000E 11	-1.23200E 12	1.22000E 11	2.04000E 00	2.50000E-01	0.0	1.26539E 00	-6.00000E 09

NOE = 7 AA B EDGE

9.26700E 02		-2.60800E 00		1.55900E 00			
1.53500E 04		-2.78000E 00		3.09900E 01			
3.16100E 03		-2.32300E 00		4.13200E 01			
8.95100E 02		-1.98400E 00		4.95600E 01			
1.72300E 02		-1.56200E 00		6.19800E 01			
2.79300E 01		-1.12100E 00		8.26400E 01			
2.58100E 00		-5.87600E-01		1.50030E 02			

*** TEST PROBLEM NO. 1 *** TWO MATERIAL *** APPENDIX SPECTRUM

J	DX	X	FRC5	CAL	SUM CAL	FPGS/GM	VFORTY	PFNF MASS	J
1	-1.00000E-9		1.-52023E 08	3.-63171E 09	3.-63171E 09	6.-91015E 10	6.-77721E 10	2.-24400E -03	2
2	2.-02000E-03	1.-52081E 08	3.-63308E 09	7.-26479E 00	7.-26479E 00	6.-64514E 10	6.-64514E 10	2.-28888E -03	4
3	3.-06040E-03	1.-52099E 08	3.-63352E 09	1.-00983E 01	1.-00983E 01	6.-51398E 10	6.-51398E 10	2.-23466E -03	5
4	4.-12161E-03	1.-52079E 09	3.-63304E 09	1.-45313E 01	1.-45313E 01	6.-51398E 10	6.-51398E 10	2.-23466E -03	5
5	5.-20404E-03	1.-52020E 08	3.-63163E 09	1.-8'630E 01	1.-8'630E 01	6.-38377E 10	6.-38377E 10	2.-38135E -03	6
6	6.-10408E-03	1.-51921E 08	3.-62928E 09	2.-17922E 01	2.-17922E 01	6.-25474E 10	6.-25474E 10	2.-42898E -03	7
7	7.-43428E-03	1.-51784E 08	3.-62598E 09	2.-54182E 01	2.-54182E 01	6.-12634E 10	6.-12634E 10	2.-47756E -03	8
8	8.-58297E-03	1.-51606E 08	3.-62174E 09	2.-90400E 01	2.-90400E 01	5.-99919E 10	5.-99919E 10	2.-57711E -03	9
9	9.-14869E-03	1.-51389E 09	3.-61655E 09	3.-26565E 01	3.-26565E 01	5.-67314E 10	5.-67314E 10	2.-67765E -03	10
10	1.-17166E-03	9.-75463E-03	1.-51389E 09	3.-61655E 09	3.-61655E 09	5.-67314E 10	5.-67314E 10	2.-62920E -03	11
11	1.-19509E-03	1.-09497E-02	1.-51132E 08	3.-61042E 09	3.-61042E 09	5.-74871E 10	5.-74871E 10	2.-69179E -03	12
12	1.-21699E-03	1.-21687E-02	1.-50835E 08	3.-60333E 09	3.-60333E 09	5.-62443E 10	5.-62443E 10	2.-80285E -03	13
13	1.-24337E-03	1.-34121E-02	1.-50499E 08	3.-59528E 09	4.-34656E 01	5.-50184E 10	5.-50184E 10	2.-83542E -03	14
14	1.-26824E-03	1.-46803E-02	1.-50122E 08	3.-58629E 09	4.-70518E 01	5.-38047E 10	5.-38047E 10	2.-79013E -03	15
15	1.-29361E-03	1.-59739E-02	1.-49796E 08	3.-57635E 09	5.-06282E 01	5.-26034E 10	5.-26034E 10	2.-86593E -03	16
16	1.-31948E-03	1.-72934E-02	1.-49250E 08	3.-56546E 09	5.-41937E 01	5.-14149E 10	5.-14149E 10	2.-90091E -03	17
17	1.-34587E-03	1.-86393E-02	1.-48755E 08	3.-55362E 09	5.-77473E 01	5.-02395E 10	5.-02395E 10	2.-69089E -03	18
18	1.-37277E-03	2.-00121E-02	1.-48220E 08	3.-54085E 09	6.-12881E 01	4.-90774E 10	4.-90774E 10	3.-C2013E -03	19
19	1.-40024E-03	2.-14123E-02	1.-47646E 08	3.-52714E 09	6.-48153E 01	4.-79288E 10	4.-79288E 10	3.-08053E -03	20
20	1.-42825E-03	2.-28405E-02	1.-47033E 08	3.-51250E 09	6.-83278E 01	4.-67940E 10	4.-67940E 10	3.-14214E -03	21
21	1.-45661E-03	2.-42974E-02	1.-46382E 08	3.-49694E 09	7.-18247E 01	4.-56732E 10	4.-56732E 10	1.-23498E -03	22
22	1.-48595E-03	2.-57833E-02	1.-45692E 08	3.-48047E 09	7.-53052E 01	4.-45667E 10	4.-45667E 10	3.-69089E -03	23
23	1.-51567E-03	2.-72990E-02	1.-44965E 08	3.-46309E 09	7.-87683E 01	4.-34747E 10	4.-34747E 10	3.-33447E -03	24
24	1.-54598E-03	2.-88450E-02	1.-44200E 08	3.-44482E 09	8.-22131E 01	4.-23974E 10	4.-23974E 10	3.-40116E -03	25
25	1.-57690E-03	3.-04219E-02	1.-43398E 08	3.-42566E 09	8.-56387E 01	4.-13348E 10	4.-13348E 10	3.-46911E -03	26
26	1.-60844E-03	3.-20303E-02	1.-42559E 08	3.-40562E 09	8.-90444E 01	4.-02874E 10	4.-02874E 10	3.-38568E -03	27
27	1.-64061E-03	3.-36709E-02	1.-41685E 08	3.-38473E 09	9.-24291E 01	3.-92551E 10	3.-92551E 10	3.-60931E -03	28
28	1.-67342E-03	3.-53443E-02	1.-40774E 08	3.-36298E 09	9.-57921E 01	3.-82391E 10	3.-82391E 10	3.-61526E -03	29
29	1.-70689E-03	3.-70512E-02	1.-39829E 08	3.-34040E 09	9.-91251E 01	3.-72366E 10	3.-72366E 10	3.-75515E -03	30
30	1.-74102E-03	3.-87922E-02	1.-38850E 08	3.-31700E 09	1.-02449E 02	3.-62508E 10	3.-62508E 10	1.-83025E -03	31
31	1.-77584E-03	4.-05681E-02	1.-37836E 08	3.-29279E 09	1.-05742E 02	3.-52806E 10	3.-52806E 10	3.-90586E -03	32
32	1.-81136E-03	4.-23794E-02	1.-36790E 08	3.-26780E 09	1.-09010E 02	3.-43262E 10	3.-43262E 10	3.-98500E -03	33
33	1.-84759E-03	4.-42270E-02	1.-35711E 08	3.-24203E 09	1.-12252E 02	3.-33878E 10	3.-33878E 10	4.-06470E -03	34
34	1.-88454E-03	4.-61116E-02	1.-34601E 08	3.-21550E 09	1.-15468E 02	3.-24853E 10	3.-24853E 10	4.-14599E -03	35
35	1.-92223E-03	4.-80338E-02	1.-33460E 08	3.-18824E 09	1.-18656E 02	3.-15589E 10	3.-15589E 10	4.-22891E -03	36
36	1.-96068E-03	4.-99945E-02	1.-32289E 08	3.-16026E 09	1.-21816E 02	3.-06686E 10	3.-06686E 10	4.-31349E -03	37
37	1.-9989E-03	5.-19944E-02	1.-31089E 08	3.-13158E 09	1.-24948E 02	2.-97944E 10	2.-97944E 10	4.-39976E -03	38
38	2.-03989E-03	5.-40343E-02	1.-29459E 08	3.-10223E 09	1.-28050E 02	2.-89364E 10	2.-89364E 10	4.-47775E -03	39
39	2.-08069E-03	5.-61146E-02	1.-28503E 08	3.-07221E 09	1.-31122E 02	2.-80945E 10	2.-80945E 10	4.-64944E -03	40
40	2.-12230E-03	5.-82372E-02	1.-27320E 08	3.-04156E 09	1.-34164E 02	2.-72688E 10	2.-72688E 10	4.-69096E -03	41
41	2.-16474E-03	6.-04020E-02	1.-26011E 08	3.-01029E 09	1.-37174E 02	2.-64593E 10	2.-64593E 10	4.-75244E -03	42
42	2.-20804E-03	6.-26100E-02	1.-24677E 08	2.-97843E 00	1.-40152E 02	2.-56659E 10	2.-56659E 10	4.-85789E -03	43
43	2.-25220E-03	6.-48622E-02	1.-23319E 08	2.-94630E 00	1.-43093E 02	2.-48887E 10	2.-48887E 10	4.-95494E -03	44
44	2.-29724E-03	6.-71595E-02	1.-21939E 08	2.-91302E 00	1.-46011E 02	2.-41275E 10	2.-41275E 10	5.-10394E -03	45
45	2.-34319E-03	6.-95027E-02	1.-20536E 08	2.-87951E 00	1.-48891E 02	2.-33875E 10	2.-33875E 10	5.-15602E -03	46
46	2.-39005E-03	7.-18927E-02	1.-19134E 08	2.-84551E 00	1.-51736E 02	2.-26531E 10	2.-26531E 10	5.-25812E -03	47
47	2.-43785E-03	7.-43306E-02	1.-17669E 08	2.-81102E 00	1.-54547E 02	2.-19198E 10	2.-19198E 10	5.-36328E -03	48
48	2.-48661E-03	7.-68172E-02	1.-16207E 08	2.-77609E 00	1.-57324E 02	2.-12423E 10	2.-12423E 10	5.-47054E -03	49
49	2.-53634E-03	7.-93535E-02	1.-16727E 08	2.-74073E 00	1.-60664E 02	2.-05605E 10	2.-05605E 10	5.-57996E -03	50
50	2.-58707E-03	8.-19406E-02	1.-12305E 08	2.-70496E 00	1.-62769E 02	1.-93943E 10	1.-93943E 10	5.-67915E -03	

*** TEST PROBLEM NO. 1 *** TWO MATERIAL *** ARBITRARY SPECTRUM

J	DX	X	ERGS	CAL	SUM CAL	ERGS/GM	VELOCITY	LONG. MASS.	3
51	2.633891E-03	8.45794E-02	1.11717E 08	2.66881E 00	1.65438E 02	1.92436E 10	5.80539E-03	51	
52	2.69159E-03	8.72710E-02	1.10189E 08	2.63231E 00	1.68070E 02	1.86083E 10	5.92149E-03	52	
53	2.74542E-03	9.00164E-02	1.08647E 08	2.59549E 00	1.70666E 02	1.79882E 10	6.03097E-03	53	
54	2.80033E-03	9.28167E-02	1.07093F 08	2.55836E 00	1.73224E 02	1.73832E 10	6.16072E-03	54	
55	2.85633E-03	9.56731E-02	1.05527E 08	2.52035E 00	1.75745E 02	1.67931C 10	6.29139E-03	55	
56	2.91346E-03	9.85865E-02	1.03950E 08	2.48329E 00	1.78228E 02	1.62179E 10	6.40942E-03	56	
57	2.97173E-03	1.01558E-01	1.02364E 08	2.44440E 00	1.80674E 02	1.56573E 10	6.53178E-03	57	
58	3.03117E-03	1.04589E-01	1.00770E 08	2.40730E 00	1.83081E 02	1.51111E 10	6.664356E-03	58	
59	3.09179E-03	1.07681E-01	9.91676F 07	2.36903E 00	1.85450E 02	1.45793E 10	6.80193E-03	59	
60	3.15362E-03	1.10835E-01	9.75592E 07	2.33016E 00	1.87781E 02	1.40616E 10	6.93797E-03	60	
61	3.21670E-03	1.14052E-01	9.59453E 07	2.29205E 00	1.90073E 02	1.35579E 10	7.07673E-03	61	
62	3.28103E-03	1.17333E-01	9.43271E 07	2.25339F 00	1.92326E 02	1.30678E 10	7.21627E-03	62	
63	3.34665E-03	1.20679E-01	9.27055E 07	2.21466E 00	1.94541E 02	1.25913E 10	7.36764E-03	63	
64	3.41358E-03	1.24093E-01	9.10815E 07	2.17586E 00	1.96717E 02	1.21282E 10	7.50499E-03	64	
65	3.48106E-03	1.27575E-01	8.94562E 07	2.13703E 00	1.98854E 02	1.16782E 10	7.66008E-03	65	
66	3.55149E-03	1.31126E-01	8.79305E 07	2.09820E 00	2.00952E 02	1.12412E 10	7.81129E-03	66	
67	3.62252E-03	1.34749E-01	8.62053F 07	2.05937E 00	2.03011E 02	1.08168E 10	8.62050F-03	67	
68	3.69497E-03	1.38444E-01	8.45817E 07	2.02058E 00	2.05032E 02	1.04050E 10	8.12894E-03	68	
69	3.76887E-03	1.422213E-01	8.29605E 07	1.98188E 00	2.07014E 02	1.00055E 10	8.29152E-03	69	
70	3.84425E-03	1.46057E-01	8.13426E 07	1.94321E 00	2.08957E 02	9.61798E 09	8.45735E-03	70	
71	3.92114E-03	1.49978E-01	7.97290F 07	1.90466E 00	2.10842E 02	9.24234E 09	8.62050F-03	71	
72	3.99956E-03	1.53977E-01	7.81206E 07	1.86623E 00	2.12728E 02	8.7832E 09	8.79463E-03	72	
73	4.07955E-03	1.58057E-01	7.65181E 07	1.82795E 00	2.14556E 02	8.52569E 09	8.97501E-03	73	
74	4.16114E-03	1.622213E-01	7.49224E 07	1.78903E 00	2.16346E 02	8.18421E 09	9.15451E-03	74	
75	4.24436E-03	1.66463E-01	7.33334E 07	1.75190E 00	2.18098E 02	7.85316E 09	9.33760E-03	75	
76	4.32925E-03	1.70792E-01	7.17549E 07	1.71416E 00	2.19812E 02	7.53383E 09	9.52635E-03	76	
77	4.41584E-03	1.75208E-01	7.01845E 07	1.67665E 00	2.21488E 02	7.22447E 09	9.71484E-03	77	
78	4.50415E-03	1.79712E-01	6.86241E 07	1.63737E 00	2.23128E 02	6.92534E 09	9.90613E-03	78	
79	4.59424E-03	1.84306E-01	6.70745E 07	1.60235E 00	2.24730E 02	6.63623E 09	1.01073E-02	79	
80	4.68612E-03	1.88992E-01	6.55362E 07	1.56560E 00	2.26296E 02	6.35690E 09	1.03095E-02	80	
81	4.77984E-03	1.93772E-01	6.40100E 07	1.52915E 00	2.27825E 02	6.08712E 09	1.05157E-02	81	
82	4.87544E-03	1.986647E-01	6.24966E 07	1.49299E 00	2.29318E 02	5.826667E 09	1.07260E-02	82	
83	4.87544E-04	1.99135E-01	7.06529E 07	1.68879E 00	2.31007E 02	5.37229E 10	1.31588E-01	83	
84	5.02170E-04	1.99637E-01	6.91732E 07	1.65251E 00	2.32659E 02	5.10376E 10	1.35536E-01	84	
85	5.17235E-04	2.00154E-01	6.76286E 07	1.61559E 00	2.34092E 02	4.84439E 10	1.27602E-01	85	
86	5.32752E-04	2.00687E-01	6.60508E 07	1.57809E 00	2.35853E 02	4.59412E 10	1.47479E-01	86	
87	5.48735E-04	2.01236E-01	6.44675E 07	1.54007E 00	2.37393E 02	4.35287E 10	1.48104E-01	87	
88	5.65197E-04	2.01801E-01	6.318575E 07	1.50161E 00	2.38894E 02	4.12054E 10	1.52544E-01	88	
89	5.82153E-04	2.02383E-01	6.12316E 07	1.46227E 00	2.40357E 02	4.84439E 10	1.57123E-01	89	
90	5.99918E-04	2.02983E-01	5.95925E 07	1.42361E 00	2.41781E 02	5.68226E 10	1.61817E-01	90	
91	6.17606F-04	2.03600E-01	5.79431E 07	1.38421E 00	2.43165E 02	5.47606E 10	1.66692E-01	91	
92	6.36124E-04	2.04237E-01	5.62860E 07	1.34463E 00	2.44510E 02	5.27830E 10	1.71693E-01	92	
93	6.55218E-04	2.04892E-01	5.46241E 07	1.30492E 00	2.45815E 02	5.08944E 10	1.76843E-01	93	
94	6.74875E-04	2.05567E-01	5.29601E 07	1.26517E 00	2.47080E 02	4.90752E 10	1.82149E-01	94	
95	6.95121E-04	2.06262E-01	5.12967F 07	1.22554E 00	2.48305E 02	4.73418F 10	1.87613E-01	95	
96	7.15975E-04	2.06978E-01	4.96367E 07	1.18578E 00	2.49491E 02	4.56863E 10	1.93242E-01	96	
97	7.37454E-04	2.07715E-01	4.79825E 07	1.14626E 00	2.50637E 02	4.41071E 10	1.99039E-01	97	
98	7.59578E-04	2.08475E-01	4.63368E 07	1.10695E 00	2.51744E 02	4.26022E 10	2.05010E-01	98	
99	7.82365E-04	2.09257E-01	4.47021E 07	1.06789E 00	2.52812E 02	2.11697E 10	2.11160F-01	99	
100	8.05836E-04	2.10063E-01	4.30808E 07	1.02916E 00	2.53841E 02	1.98077E 10	2.17495E-03	100	

*** TEST PROBLEM NO. 1 *** TWO MATERIAL *** ARBITRARY SPECTRUM

<i>i</i>	<i>DX</i>	<i>X</i>	FRGS	CAL	SUM CAL	FRGS/5M	VFLNCY	ONE MASS
101	8.30011E-04	2.13893E-01	4.14753E-07	9.90309E-01	2.54832E-02	1.85141E-10	0	2.240206E-03 101
102	8.54911E-04	2.11748E-01	1.98473E-07	9.52887E-01	2.55178E-02	1.72859E-10	0	2.30741E-03 101
103	8.80559E-04	2.12628E-01	3.83207E-07	9.15449E-01	2.56700E-02	1.61240E-10	0	2.37663E-03 101
104	9.06975E-04	2.13535E-01	3.67759E-07	8.78545E-01	2.57579E-02	1.50233E-10	0	2.44793E-03 104
105	9.34185E-04	2.14470E-01	3.52555E-07	8.42233E-01	2.58421E-02	1.39827E-10	0	2.52136E-03 105
106	9.62210E-04	2.15432E-01	3.37613E-07	8.76529E-01	2.59228E-02	1.30001E-10	0	2.59701E-03 106
107	9.91076E-04	2.16423E-01	3.22952E-07	7.71505E-01	2.59999E-02	1.20733E-10	0	2.67492E-03 107
108	1.02081E-03	2.17444E-01	3.08588E-07	7.37191E-01	2.60736E-02	1.12004E-10	0	2.75916E-03 108
109	1.05143E-03	2.18495E-01	2.94537E-07	7.03624E-01	2.61440E-02	1.03790E-10	0	2.83782E-03 109
110	1.08298E-03	2.19578E-01	2.80813E-07	6.70839E-01	2.62111E-02	9.60717E-09	0	2.92295E-03 110
111	1.11547E-03	2.20694E-01	2.67429E-07	6.38866E-01	2.62750E-02	8.88281E-09	0	3.01064E-03 111
112	1.14893E-03	2.21843E-01	2.54398E-07	6.07735E-01	2.63357E-02	9.20385E-09	0	3.10096E-03 112
113	1.18340E-03	2.23026E-01	2.41729E-07	5.77471E-01	2.63935E-02	7.56825E-09	0	3.19399E-03 113
114	1.21890E-03	2.24245E-01	2.29432E-07	5.48094E-01	2.64483E-02	6.97403E-09	0	3.29041E-03 114
115	1.25547E-03	2.25500E-01	2.17513E-07	5.19625E-01	2.65003E-02	6.41921E-09	0	3.38450E-03 115
116	1.29313E-03	2.26793E-01	2.05984E-07	4.92079E-01	2.65495E-02	5.90186E-09	0	3.49016E-03 116
117	1.33192E-03	2.28125E-01	1.94845E-07	4.65468E-01	2.65960E-02	5.42009E-09	0	3.59496E-03 117
118	1.37188E-03	2.29497E-01	1.84101E-07	4.39801E-01	2.66400E-02	4.97206E-09	0	3.70271E-03 118
119	1.41304E-03	2.30910E-01	1.73755F-07	4.15085E-01	2.66815E-02	4.55596E-09	0	3.81370E-03 119
120	1.45543E-03	2.32366E-01	1.63807E-07	3.91322E-01	2.67206E-02	4.17003E-09	0	3.92820E-03 120
121	1.49909E-03	2.33865E-01	1.54259E-07	3.68512E-01	2.67575E-02	3.81259E-09	0	4.04605E-03 121
122	1.54406E-03	2.35409E-01	1.45103E-07	3.46652E-01	2.67922E-02	3.48197E-09	0	4.16744E-03 122
123	1.59039E-03	2.36999E-01	1.36353E-07	3.25736E-01	2.68247E-02	3.17658E-09	0	4.29245E-03 123
124	1.63810E-03	2.38637E-01	1.27989E-07	3.05754E-01	2.68553E-02	2.89487E-09	0	4.42123E-03 124
125	1.68724E-03	2.40325E-01	1.20011E-07	2.86695E-01	2.68840E-02	2.63534E-09	0	4.55338E-03 125
126	1.73786E-03	2.42062E-01	1.12413E-07	2.668545E-01	2.69108E-02	2.39662E-09	0	4.69044E-03 126
127	1.78999E-03	2.43852E-01	1.05108E-07	2.51286E-01	2.69360E-02	2.17727E-09	0	4.83119E-03 127
128	1.84369E-03	2.45569E-01	9.83291E-08	2.34900E-01	2.69595E-02	1.97601E-09	0	4.97613E-03 128
129	1.89900E-03	2.47595E-01	9.19264E-08	1.93365E-01	2.69814E-02	1.79150E-09	0	5.12641E-03 129
130	1.95598E-03	2.49551E-01	8.56706E-08	1.53613E-01	2.70019E-02	1.62280E-09	0	5.27918E-03 130
131	2.01465E-03	2.51566E-01	7.98515E-08	1.30759E-01	2.70209E-02	1.46852E-09	0	5.44755E-03 131
132	2.07509E-03	2.53641E-01	7.43581E-08	1.77635E-01	2.70387E-02	1.32766E-09	0	5.62068E-03 132
133	2.13735E-03	2.55778E-01	6.91790E-08	1.65263E-01	2.70552E-02	1.19921E-09	0	5.76870E-03 133
134	2.20147E-03	2.57980E-01	6.43024E-08	1.53613E-01	2.70706E-02	1.08221E-09	0	5.94176E-03 134
135	2.26751E-03	2.60247E-01	5.97162E-08	1.42657E-01	2.70849E-02	9.75753E-08	0	6.12001E-03 135
136	2.33554E-03	2.62583E-01	5.54081E-08	1.32365E-01	2.70981E-02	8.78989E-08	0	6.30361E-03 136
137	2.40560E-03	2.64988E-01	5.13655E-08	1.22708E-01	2.71104E-02	7.91125E-08	0	6.49272E-03 137
138	2.47777E-03	2.67466E-01	4.75760E-08	1.13655E-01	2.71217E-02	7.11417E-08	0	6.64750E-03 138
139	2.55210E-03	2.70018E-01	4.40272E-08	1.05177E-01	2.71322E-02	6.39175E-08	0	6.82814E-03 139
140	2.62867E-03	2.72647E-01	4.07066E-08	9.72446E-02	2.71420E-02	5.73754E-08	0	7.09477E-03 140
141	2.70753E-03	2.75354E-01	3.76022E-08	8.98285E-02	2.71509E-02	5.14567E-08	0	7.31761E-03 141
142	2.78875E-03	2.78143E-01	3.47921E-08	8.29005E-02	2.71592E-02	4.61045E-08	0	7.52686E-03 142
143	2.87242E-03	2.81016E-01	3.19949E-08	7.64331E-02	2.71669E-02	4.12696E-08	0	7.75266E-03 143
144	2.95859E-03	2.83974E-01	2.94694E-08	7.0399AE-02	2.71739E-02	3.69048E-08	0	7.99423E-03 144
145	3.04735E-03	2.87021E-01	2.7148E-08	6.47750E-02	2.71804E-02	3.29672E-08	0	8.22473E-03 145
146	3.13877E-03	2.90160E-01	2.49211E-08	5.95143E-02	2.71963E-02	2.94174E-08	0	8.47153E-03 146
147	3.23293E-03	2.93393E-01	2.28733E-08	5.46544E-02	2.7191AE-02	2.62194E-08	0	8.72563E-03 147
148	3.32992E-03	2.96723E-01	2.0973F-08	5.01130E-02	2.71984E-02	2.33470E-08	0	9.29744E-03 148
149	3.42991E-03	3.00153E-01	1.92093E-08	4.58894E-02	2.72014E-02	2.07510E-08	0	9.75707E-03 149
150	3.53271E-03	3.03686E-01	1.75660E-08	4.19638E-02	2.72056E-02	1.84231E-08	0	9.94723E-03 150

*** TEST PROBLEM NO. 1 *** TWO MATERIAL *** ARBITRARY SPECTRUM

J UX X FRS FAL SUM CAL ERGSEG VFL DCLTY CONF MERS J

151	3.63869E-03	3.07324E-01	1.60398E 06	3.93177E-02	2.72094E 02	1.63324E 08	0	9.92097E-03 151
152	3.74785E-03	3.11072E-01	1.46233E 06	3.49337E-02	2.72129E 02	1.644564E 08	0	1.01154E-02 152
153	3.86029E-03	3.14932E-01	1.33996E 06	3.17956E-02	2.72161E 02	1.27745E 08	0	1.04189E-02 153
154	3.97609E-03	3.16909E-01	1.20926E 06	2.88882E-02	2.72190E 02	1.12683E 08	0	1.07315E-02 154
155	4.09538E-03	3.23004E-01	1.09662E 06	2.51973E-02	2.72216E 02	9.92107E 07	0	1.10534E-02 155
156	4.21824E-03	3.27222E-01	9.92481E 05	2.37095E-02	2.72240E 02	8.71743E 07	0	1.18505E-02 156
157	4.34479E-03	3.31567E-01	8.96331E 05	2.14126E-02	2.72261E 02	7.64250E 07	0	1.17266E-02 157
158	4.47513E-03	3.36042E-01	8.07679E 05	1.92948E-02	2.72281E 02	6.68698E 07	0	1.20784E-02 158
159	4.60938E-03	3.40651E-01	7.26069E 05	1.73451E-02	2.72299E 02	5.83622E 07	0	1.24407E-02 159
160	4.74766E-03	3.45399E-01	6.51069E 05	1.55535E-02	2.72314E 02	5.08094E 07	0	1.28139E-02 160
161	4.89009E-03	3.50289E-01	5.82755E 05	1.39109E-02	2.72327E 02	4.41172E 07	0	1.31984E-02 161
162	5.03680E-03	3.55326E-01	5.19302E 05	1.24057E-02	2.72340E 02	3.81999E 07	0	1.35843E-02 162
163	5.18790E-03	3.60514E-01	4.61787E 05	1.10317E-02	2.72351E 02	3.29779E 07	0	1.40032E-02 163
164	5.34354E-03	3.65857E-01	4.09382E 05	9.77979E-03	2.72361E 02	2.83855E 07	0	1.44227E-02 164
165	5.50284E-03	3.71361E-01	3.61759E 05	8.64208E-03	2.72369E 02	2.43525E 07	0	1.48549E-02 165
166	5.66896E-03	3.77030E-01	3.18597E 05	7.61102E-03	2.72377E 02	2.08226E 07	0	1.53005E-02 166
167	5.83903E-03	3.82869E-01	2.79598E 05	6.67936E-03	2.72384E 02	1.77415E 07	0	1.57595E-02 167
168	6.01420E-03	3.88883E-01	2.44470E 05	5.94019E-03	2.72389E 02	1.50607E 07	0	1.62324E-02 168
169	6.19463E-03	3.95078E-01	2.19293E 05	5.08644E-03	2.72395E 02	1.27395E 07	0	1.47193E-02 169
170	6.38046E-03	4.01459E-01	1.84725E 05	4.41295E-03	2.72399E 02	1.07264E 07	0	1.27209E-02 170
171	6.57168E-03	4.08030E-01	1.59584E 05	3.81231E-03	2.72403F 02	8.99696E 06	0	1.77375E-02 171
172	6.76903E-03	4.14799E-01	1.37265E 05	3.27914E-03	2.72406F 02	7.51329E 06	0	1.22605E-02 172
173	6.97211E-03	4.21772E-01	1.17534E 05	2.80779E-03	2.72409E 02	6.24593E 06	0	1.38177E-02 173
174	7.18127E-03	4.288953E-01	1.00166E 05	2.39289E-03	2.72411E 02	5.16795E 06	0	1.93822E-02 174
175	7.39671E-03	4.36350E-01	8.49483E 04	2.02934E-03	2.72413E 02	4.25514E 06	0	1.39637E-02 175
176	7.61861E-03	4.43968E-01	7.16768E 04	1.71230E-03	2.72415E 02	3.48574E 06	0	2.35526E-02 176
177	7.84717E-03	4.51815E-01	6.01604F 04	1.43719E-03	2.72416E 02	2.84050E 06	0	2.11795E-02 177
178	8.08258E-03	4.59898E-01	5.02185E 04	1.19968E-03	2.72418E 02	2.30203F 06	0	2.18149E-02 178
179	8.32506E-03	4.68223E-01	4.162821F 04	9.95750E-04	2.72419F 02	1.85507F 06	0	2.46691E-02 179
180	8.57481E-03	4.76798E-01	3.43937E 04	8.21637E-04	2.72419E 02	1.48611E 06	0	2.31434E-02 180
181	8.83205E-03	4.85630E-01	2.82071E 04	6.73845E-04	2.72420E 02	1.18330E 06	0	2.18377E-02 181
182	9.09702E-03	4.94727E-01	2.29876E 04	5.49155E-04	2.72421E 02	9.36252E 05	0	2.45528E-02 182
183	9.36993E-03	5.04097E-01	1.86611E 04	4.44621E-04	2.72421E 02	7.35952E 05	0	2.52804E-02 183
184	9.65102E-03	5.13748E-01	1.49673F 04	3.57555E-04	2.72421E 02	5.74602F 05	0	2.60481E-02 184
185	9.94056E-03	5.23688E-01	1.19523F 04	2.85531E-04	2.72422E 02	4.45491E 05	0	2.58296E-02 185
186	1.02388E-02	5.33927E-01	9.47581E 03	2.26369E-04	2.72422E 02	3.42899E 05	0	2.75134E-02 186
187	1.05459E-02	5.44473E-01	7.45634E 03	1.78126E-04	2.72422E 02	2.61962E 05	0	2.44635E-02 187
188	1.06623E-02	5.55335E-01	5.82199E 03	1.39082E-04	2.72421E 02	1.98585E 05	0	2.93174E-02 188
189	1.11882E-02	5.66524E-01	4.50963E 03	1.07731E-04	2.72422E 02	1.49341E 05	0	3.01984E-02 189
190	1.15238E-02	5.78047E-01	3.46433F 03	8.27599E-05	2.72422E 02	1.11383E 05	0	2.10244E-02 190
191	1.18695E-02	5.89917E-01	2.63869E 03	6.30361E-05	2.72423E 02	8.23667E 04	0	3.03585E-02 191
192	1.22256E-02	6.02143E-01	1.99218E 03	4.75914E-05	2.72423E 02	6.03745E 04	0	3.13970E-02 192
193	1.25924E-02	6.14735E-01	1.49043E 03	3.56052E-05	2.72423E 02	4.38532E 04	0	3.19869E-02 193
194	1.29702E-02	6.27705E-01	1.10463E 03	2.63886E-05	2.72423E 02	3.15550E 04	0	3.40665E-02 194
195	1.335593E-02	6.40644E-01	8.10759E 02	1.93691E-05	2.72423E 02	2.24865E 04	0	3.60567E-02 195
196	1.37601E-02	6.54824E-01	5.89189E 02	1.40752E-05	2.72423E 02	1.58647E 04	0	3.14844E-02 196
197	1.41729E-02	6.68997E-01	4.23759E 02	1.01232E-05	2.72423E 02	1.10779E 04	0	3.82525E-02 197
198	1.45980E-02	6.83595E-01	0.0	0	2.72423E 02	0	3.04001E-02 198	
199	1.50360E-02	6.98631E-01	0.0	0	2.72423E 02	0	4.05421E-02 199	
200	1.54871E-02	7.14118E-01	0.0	0	2.72423E 02	0	4.17396E-02 200	

*** TEST PROBLEM NO. 1 *** TWO MATERIAL *** ARBITRARY SPECTRUM

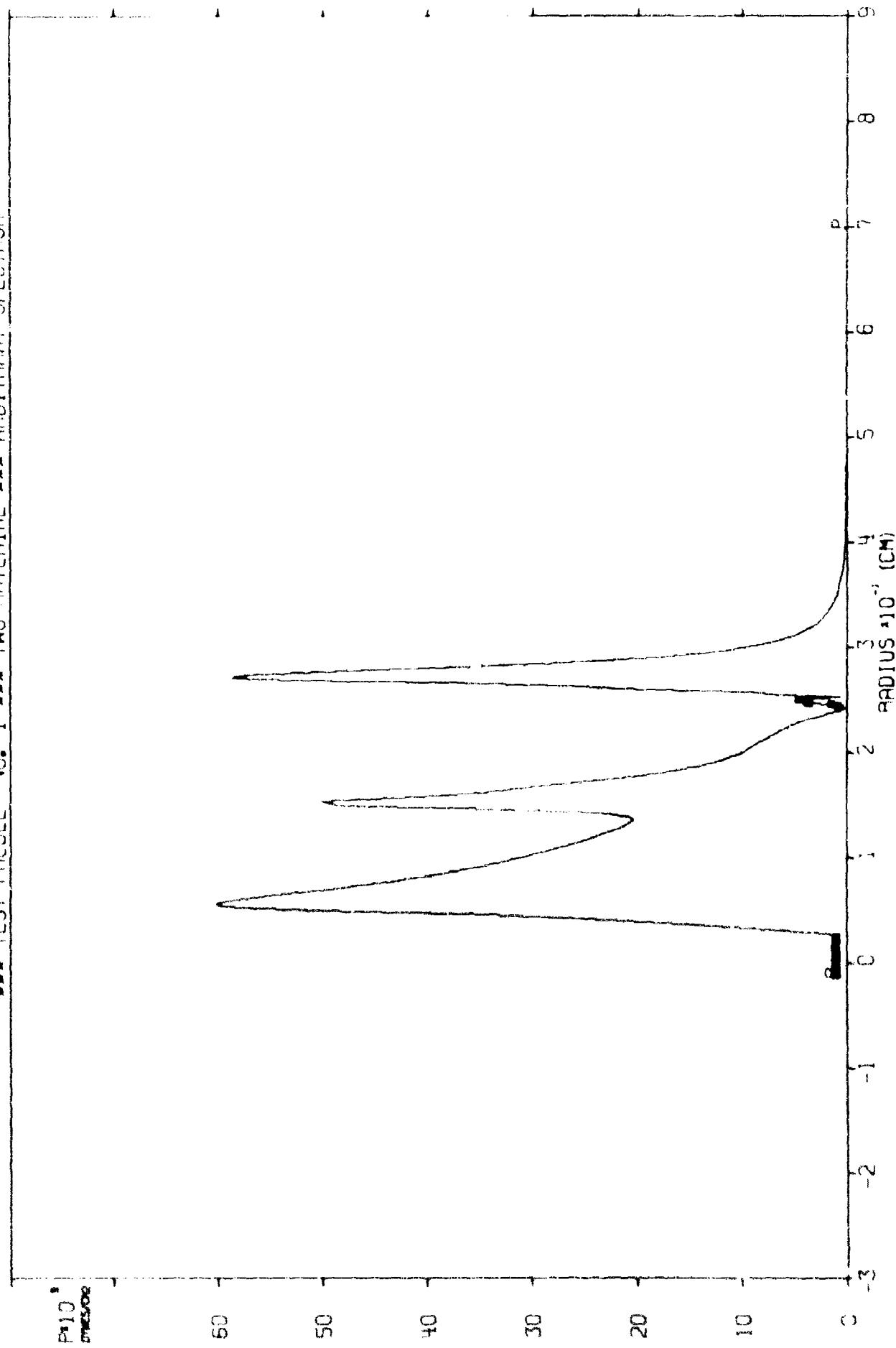
J	Dx	X	ERGS	CAL	SUM CAL	ERCS/GW	VELOCITY	ZONE MASS	J
201	1.59517E-02	7.30070E-01	0	2.72423E 02	201	4.30536E-02	4.43452E-02	202	
202	1.64302E-02	7.46500E-01	0	2.72423E 02	202	4.56745E-01	4.46745E-01	203	
203	1.69231E-02	7.63423E-01	0	2.72423E 02	203	4.70458E-02	4.70458E-02	204	
204	1.74308E-02	7.80854E-01	0	2.72423E 02	204	4.84572E-02	4.84572E-02	205	
205	1.79537E-02	7.98808E-01	0	2.72423E 02	205	4.99109E-02	4.99109E-02	206	
206	1.84924E-02	8.17300E-01	0	2.72423E 02	206	5.14042E-02	5.14042E-02	207	
207	1.90471E-02	8.32347E-01	0	2.72423E 02	207	5.29506E-02	5.29506E-02	208	
208	1.96185E-02	8.55966E-01	0	2.72423E 02	208	5.45390E-02	5.45390E-02	209	
209	2.02071E-02	8.76173E-01	0	2.72423E 02	209	5.61751E-02	5.61751E-02	210	
210	2.08133E-02	8.96986E-01	0	2.72423E 02	210	5.78604E-02	5.78604E-02	211	
211	2.14377E-02	9.18424E-01	0	2.72423E 02	211	5.95962E-02	5.95962E-02	212	
212	2.20860E-02	9.40505E-01	0	2.72423E 02	212	6.13841E-02	6.13841E-02	213	
213	2.27433E-02	9.63248E-01	0	2.72423E 02	213	6.32256E-02	6.32256E-02	214	
214	2.34256E-02	9.86674E-01	0	2.72423E 02	214	6.51274E-02	6.51274E-02	215	
215	2.41283E-02	1.01080E 00	0	2.72423E 02	215	6.70761E-02	6.70761E-02	216	
216	2.48522E-02	1.03565E 00	0	2.72423E 02	216	6.90883E-02	6.90883E-02	217	
217	2.55978E-02	1.06125E 00	0	2.72423E 02	217	7.11610E-02	7.11610E-02	218	
218	2.63657E-02	1.08762E 00	0	2.72423E 02	218	7.32054E-02	7.32054E-02	219	
219	2.71567E-02	1.11477E 00	0	2.72423E 02	219	7.54944E-02	7.54944E-02	220	
220	2.79714E-02	1.14275E 00	0	2.72423E 02	220	7.77595E-02	7.77595E-02	221	
221	2.88105E-02	1.17156E 00	0	2.72423E 02	221	8.00923E-02	8.00923E-02	222	
222	2.96748E-02	1.20123E 00	0	2.72423E 02	222	8.24951E-02	8.24951E-02	223	
223	3.05651E-02	1.23180E 00	0	2.72423E 02	223	8.56344E-02	8.56344E-02	224	
224	3.14820E-02	1.26328E 00	0	2.72423E 02	224	8.85034E-02	8.85034E-02	225	
225	3.24265E-02	1.29570E 00	0	2.72423E 02	225	9.10459E-01	9.10459E-01	226	
226	3.33993E-02	1.32910E 00	0	2.72423E 02	226	9.45507E-01	9.45507E-01	227	
227	3.44012E-02	1.36351E 00	0	2.72423E 02	227	9.76376E-01	9.76376E-01	228	
228	3.54333E-02	1.39894E 00	0	2.72423E 02	228	1.00866E-01	1.00866E-01	229	
229	3.64963E-02	1.43543E 00	0	2.72423E 02	229	1.04598E-01	1.04598E-01	230	
230	3.75912E-02	1.47303E 00	0	2.72423E 02	230	1.08614E-01	1.08614E-01	231	
231	3.87189E-02	1.51174E 00	0	2.72423E 02	231	1.12147E-01	1.12147E-01	232	
232	3.98805E-02	1.55163E 00	0	2.72423E 02	232	1.16868E-01	1.16868E-01	233	
233	4.10769E-02	1.59270E 00	0	2.72423E 02	233	1.21192E-01	1.21192E-01	234	
234	4.23092E-02	1.63501E 00	0	2.72423E 02	234	1.26525E-01	1.26525E-01	235	
235	4.35785E-02	1.67859E 00	0	2.72423E 02	235	1.32380E-01	1.32380E-01	236	
236	4.48858E-02	1.72348E 00	0	2.72423E 02	236	1.36357E-01	1.36357E-01	237	
237	4.62324E-02	1.76971E 00	0	2.72423E 02	237	1.404647E-01	1.404647E-01	238	
238	4.76194E-02	1.81733E 00	0	2.72423E 02	238	1.44656E-01	1.44656E-01	239	
239	4.90479E-02	1.86638E 00	0	2.72423E 02	239	1.48995E-01	1.48995E-01	240	
240	5.05194E-02	1.91689E 00	0	2.72423E 02	240	1.53466E-01	1.53466E-01	241	
241	5.20350E-02	1.96893E 00	0	2.72423E 02	241	1.58060E-01	1.58060E-01	242	
242	5.35960E-02	2.02253E 00	0	2.72423E 02	242	1.62411E-01	1.62411E-01	243	
243	5.52039E-02	2.07773E 00	0	2.72423E 02	243	1.67696E-01	1.67696E-01	244	
244	5.68600E-02	2.13459E 00	0	2.72423E 02	244	1.72776E-01	1.72776E-01	245	
245	5.85658E-02	2.19316E 00	0	2.72423E 02	245	1.81444E-01	1.81444E-01	246	
246	6.03228E-02	2.25348E 00	0	2.72423E 02	246	1.87696E-01	1.87696E-01	247	
247	6.21327E-02	2.31561E 00	0	2.72423E 02	247	1.93776E-01	1.93776E-01	248	
248	6.39964E-02	2.37961E 00	0	2.72423E 02	248	1.97904E-01	1.97904E-01	249	
249	6.59163E-02	2.44552E 00	0	2.72423E 02	249	2.02134E-01	2.02134E-01	250	
	6.78938E-02	2.51342E 00	0	2.72423E 02	250				

*** TEST PROBLEM NO. 1 *** TWO MATERIAL *** ARBITRARY SPECTRUM

J	DX	X	ENERG.	CAL	SUM CAL	FREQ/CM	VELOCITY	ZONE MASS	J
251	6.99306E-02	2.58335E 00	0	2.72423F 02	1.88743F-01 251	0	0	0	
252	7.20286E-02	2.65538E 00	0	2.72423F 02	1.9x405F-01 252	0	0	0	
253	7.41894E-02	2.72957E 00	0	2.72423F 02	2.00237F-01 253	0	0	0	
254	7.64151E-02	2.80598E 00	0	2.72423F 02	2.06244F-01 254	0	0	0	
255	7.87075E-02	2.88469E 00	0	2.72423F 02	2.12432F-01 255	0	0	0	
256	8.10688E-02	2.96576E 00	0	2.72423F 02	2.19905F-01 256	0	0	0	
257	8.35008E-02	3.04926E 00	0	2.72423F 02	2.2531F4F-01 257	0	0	0	
258	8.60059E-02	3.13526E 00	0	2.72423F 02	2.3213nF-01 258	0	0	0	
259	8.85860E-02	3.22385E 00	0	2.72423F 02	2.39094F-01 259	0	0	0	
260	9.12436E-02	3.31509E 00	0	2.72423F 02	2.46267F-01 260	0	0	0	
261	9.39809E-02	3.40907E 00	0	2.72423F 02	2.53655F-01 261	0	0	0	
262	9.68004E-02	3.50587E 00	0	2.72423F 02	2.61264F-01 262	0	0	0	
263	9.97044E-02	3.60558E 00	0	2.72423F 02	2.69102F-01 263	0	0	0	
264	1.02695E-01	3.70827E 00	0	2.72423F 02	2.77176F-01 264	0	0	0	
265	1.05776E-01	3.81405E 00	0	2.72423F 02	2.854a0F-01 265	0	0	0	
266	1.08953E-01	3.92300E 00	0	2.72423F 02	2.94055F-01 266	0	0	0	
267	1.12218E-01	4.03522E 00	0	2.72423F 02	3.02877F-01 267	0	0	0	
268	1.15585E-01	4.15080E 00	0	2.72423F 02	3.11963F-01 268	0	0	0	
269	1.19052E-01	4.26986E 00	0	2.72423F 02	3.21322F-01 269	0	0	0	
270	1.22624E-01	4.39248E 00	0	2.72423F 02	3.30962F-01 270	0	0	0	
271	1.26303E-01	4.51878E 00	0	2.72423F 02	3.40890F-01 271	0	0	0	
272	1.30092E-01	4.64887E 00	0	2.72423F 02	3.51117F-01 272	0	0	0	
273	1.33994E-01	4.78287E 00	0	2.72423F 02	3.61651F-01 273	0	0	0	
274	1.38014E-01	4.92088E 00	0	2.72423F 02	3.72500F-01 274	0	0	0	
275	1.42155E-01	5.06304E 00	0	2.72423F 02	3.83675F-01 275	0	0	0	
276	1.46419E-01	5.20946E 00	0	2.72423F 02	3.95165F-01 276	0	0	0	
277	1.50812E-01	5.36027E 00	0	2.72423F 02	4.07041F-01 277	0	0	0	
278	1.55336E-01	5.51560E 00	0	2.72423F 02	4.19252F-01 278	0	0	0	
279	1.59996E-01	5.67560E 00	0	2.72423F 02	4.31830F-01 279	0	0	0	
280	1.64796E-01	5.84040E 00	0	2.72423F 02	4.44795F-01 280	0	0	0	
281	1.69740E-01	6.01014E 00	0	2.72423F 02	4.59128F-01 281	0	0	0	
282	1.74832E-01	6.18497E 00	0	2.72423F 02	4.71872F-01 282	0	0	0	

CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNEG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
25	4.7198E-10	7.9497E-11	175	83	4.5949E 09	1.9913E-01	-7.0702E-01	7.3859F-01	3.1565E-02
6.8695E-12	-1.5387E-10	4.2858E 00	-1.2048E 00	1.2023E 00	-5.9711E-08	1.9865E-01	0	6.1850E 00	2A2
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNEG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
50	7.1041E-09	3.0000E-10	186	89	5.0340E 10	2.0240E-01	4.3799E 01	1.3928E 02	1.6307E 02
3.6585E-09	8.7527E-10	6.4493E 01	-2.6028E 02	2.6027E 02	-1.2190E-04	1.9859E-01	0	6.1850E 00	282
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNEG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
7, 1.4604E-08	3.0000E-10	188	96	7.4505E 10	2.0706E-01	1.9282E 02	4.0224E 02	5.9507E 02	5.9507E 02
7.9866E-09	2.5881E-09	1.3258E 02	-9.1505E 02	9.1504E 02	-5.1313E-04	1.9838E-01	0	6.1850E 00	282
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNFG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
100	2.2104E-08	3.0000E-10	15, J	191	8.6487E 10	2.1109E-01	3.8071E 02	6.9457E 02	1.0753E 03
1.2433E-08	4.4019E-09	2.0067E 02	-1.7711E 03	1.7711E 03	-1.1739E-03	1.9808E-01	0	6.1850E 00	282
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNEG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
125	2.9604E-08	3.0000E-10	191	106	9.2405E 10	2.1576E-01	6.5675E 02	9.1635E 02	1.5731E 03
1.7024E-08	7.1073E-09	2.6876E 02	-2.7531E 03	2.7530E 03	-2.1088E-03	1.9775E-01	0	6.1850E 00	282
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNEG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
150	4.7895E-08	7.2876E-10	195	19	8.0638E 10	2.1764E-02	3.5406E 02	2.3624E 03	2.7165E 03
3.3688E-08	4.3908E-09	2.7149E 02	-4.6566E 03	4.6565E 03	-4.9237E-03	1.9716E-01	0	6.1850E 00	282
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNEG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
175	6.8827E-08	9.2583E-10	197	25	7.2557E 10	3.1174E-02	5.9193E 02	3.3689E 03	3.9608E 03
5.4588E-08	8.1581E-09	2.7150E 02	-5.8770E 03	5.8770E 03	-7.83100E-03	1.9688E-01	0	6.1850E 00	282
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNEG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
200	8.8289E-08	7.7466E-10	197	30	6.7043E 10	3.9970E-02	8.1549E 02	4.0846E 03	4.9001E 03
7.3089E-08	1.2164E-08	2.7151E 02	-6.5541E 03	6.5541E 03	-1.0496E-02	1.9681E-01	0	6.1850E 00	282
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNEG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
225	1.0582E-07	6.4538E-10	198	34	6.3193E 10	4.7695E-02	1.0076E 03	4.6040E 03	5.6116E 03
8.8901E-08	1.5945E-08	2.7152E 02	-7.0274E 03	7.0274E 03	-1.2777E-02	1.9682E-01	0	6.1850E 00	282
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
OTPP	OTPULS	ETOTAL	EHVNEG	EVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-ROUND	JFIN
250	1.2309E-07	6.3603E-10	198	38	6.0194E 10	5.5995E-02	1.7518E 03	4.9579E 03	6.2097E 03
1.0316E-07	2.0797E-08	2.7153E 02	-7.4190E 03	7.4190E 03	-1.4978E-02	1.9686E-01	0	6.1850E 00	282

CYCLE = 250 TIME = $1.231 \cdot 10^{-7}$
TEST PROBLEM NO. 1 *** TWO MATERIAL *** ARBITRARY SPECTRUM



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APPENDIX IV

TEST PROBLEM 2

(PUFF)

10	RH0(1)	EQSTC(1)	EQSTD(1)	EQSTE(1)	EQSTG(1)	EQSTH(1)	EQSTS(1)	PMIN(1)
	1.57	9.4+10	2.193+10	1.12+11	1.0	.25	0.	-1.+9
9	MATL(1)							
	MATL 1							
8	DX	TIME	RZ(1)					
	1.-3	1.-12	1.03					
7	JFIN	RZ(1)						
	110	109						
6	SDUR	T(1)	EE(1)	T(2)	EE(2)			
	3.-8	4	35.	8.	25.			
5	NDE(1)							
	9							

4	ANGLE							
	0.							
3	NRB	NRZC	NMTRLS	JRZL	JZPUL	NPRIN	NTAPE	
	2	1	1	1	20	40	26	25
2	DISCF(I), I = 1,10							
	*** TEST PROBLEM NO 2 *** TWO BLACK BODY SPECTRUM ***							

TABLE DECK FOR PROBLEM 2

1	NHNU	NTEDT	NJEDIT	LZHIZ				
	0	0	0	0				

17	JCYCS 550	NTEST 30						
16	CKP 7	TS 1.-6						
15	AA(1,9) 2.3134	B(1,9) -5.7037-1	EDGE(1,9) 1.50+2					
14	B(1,8) -2.1308	EDGE(1,6) 4.1320+1	AA(1,7) 1.0427+2	B(1,7) -1.5074	EDGE(1,7) 4.9584+1	AA(1,8) 1.6230+1	B(1,8) -1.0334	EDGE(1,8) 6.1980+1
13	EDGE(1,3) 5.32-1	AA(1,4) 2.9339+3	B(1,4) -2.8099	EDGE(1,4) 1.8424	AA(1,5) 9.0442+3	B(1,5) -2.8151	EDGE(1,5) 1.2396+1	AA(1,6) 1.0073+3
12	AA(1,1) 9.0515+2	B(1,1) -2.4056	EDGE(1,1) 1.18-1	AA(1,2) 7.1461+2	B(1,2) -2.6191	EDGE(1,2) 2.84-1	AA(1,3) 9.971+2	B(1,3) -2.5885
11	CUSPI(1) 0.	CUSPA(1) 0.	CUSPC(1) C.	CUSPD(1) 0.	CUSPG(1) 0.	CUSPS(1) 0.		

TABLE DECK POP COUNT FIGURE 2

FORMAT 8.10.3

.629	.812	.946	1.06	1.15	1.24	1.32	1.40	TBL.CAPP.1
1.47	1.53	1.60	1.66	1.72	1.78	1.83	1.89	TBL.CAPP.2
1.94	1.99	2.05	2.10	2.15	2.20	2.24	2.29	TBL.CAPP.3
2.34	2.39	2.43	2.48	2.53	2.57	2.62	2.67	TBL.CAPP.4
2.71	2.76	2.80	2.85	2.89	2.94	2.99	3.03	TBL.CAPP.5
3.08	3.12	3.17	3.22	3.26	3.31	3.36	3.41	TBL.CAPP.6
3.45	3.50	3.55	3.60	3.65	3.70	3.75	3.80	TBL.CAPP.7
3.86	3.91	3.96	4.02	4.07	4.13	4.18	4.24	TBL.CAPP.8
4.30	4.36	4.42	4.48	4.53	4.61	4.68	4.75	TBL.CAPP.9
4.82	4.89	4.97	5.04	5.12	5.20	5.29	5.38	TBL.CAPP.10
5.47	5.56	5.66	5.77	5.88	6.00	6.12	6.26	TBL.CAPP.11
6.40	6.55	6.72	6.91	7.12	7.36	7.63	7.97	TBL.CAPP.12
8.39	8.97	9.94	10.1	10.2	10.4	10.6	10.9	TBL.CAPP.13
11.2	11.6	12.1	13.0	15.0				

INPUT PARAMETERS FOR -

** TEST PROBLEM NO. 2 ** TWO BLACK BODY SPECTRA **
** THIS PROBLEM WAS RUN ON PUFF/1504 **

TABLE VALUES

NBB	NRIC	NMTRIS	JRZL	JIPUL	NPRIN	ANGLE
2	1	1	20	40	25	1.000E 00

ETTGT = 0
LGZHIZ = 0

ZONING CONSTANTS

RATIO 1.030E 00 TO ZONE 109

BLACK BODY TEMPERATURE AND ASSOCIATED ENERGY

TEMPERATURE	ENERGY
4.000E 00	3.500E 01
6.000E 00	2.500E 01

JFIN	JCYCS	NTEST	NTAPE	CKP	TS	TIME	SOUR
110	550	30	25	7.000E-01	1.000E-06	1.000F-12	3.000E-08

MATERIAL PROPERTIES FOR WALL 1
 MATERIAL THICKNESS = 8.025E-01
 FROM j = 1 TO j = 110
 9.40000E 10 2.19300E 10 1.12000E 11 1.00000E 00 2.50000E-01
 EOSTC EOSTC EOSTC EOSTC EOSTC
 9.05150E 02 -2.40560E 00 1.18000E-01
 7.14610E 02 -2.61910E 00 2.64000E-01
 9.97100E 02 -2.98850E 00 5.32000E-01
 2.93390E 03 -2.80905E 00 1.84240E 00
 9.04420E 03 -2.91510E 20 1.23960E 01
 1.004730E 03 -2.13040E 50 4.13200E 01
 1.042270E 02 1.00740E 00 4.95840E 01
 1.62300E 01 -1.03340E 00 6.19800E 01
 2.31340E 00 -5.70370E-01 1.50000E 02

EDGE

b

a

NODE = 6

J	Dx	FRGS	CAL	SUN CAL	ERGS/GM	ZONE MASS
2	1.00000E+03	5.57191E-07	1.33108E-00	1.33108E-00	3.54898E-10	2
3	1.03007E+03	2.03000E-03	4.61541E-07	1.05430E-00	2.39589E-00	1.61710E-03
4	1.06090E+03	3.09090E-03	3.78977E-07	9.05391E-01	3.29128E-00	1.66461E-03
5	1.09273E+03	4.18363E-03	3.40457E-07	8.13322E-01	4.10460E-00	1.78450E-03
6	1.12551E+03	5.30314E-03	3.13833E-07	7.49721E-01	4.85432E-00	1.77603E-03
7	1.15927E+03	6.46841E-03	2.93869E-07	7.02025E-01	5.55635E-00	1.92006E-03
8	1.19405E+03	7.66246E-03	2.78075F-07	6.64299E-01	6.22064E-00	1.87466E-03
9	1.22987E+03	8.89234E-03	2.65148E-07	6.33416E-01	6.95406E-00	1.93098E-03
10	1.26677E+03	1.01591E-02	2.54314E-07	6.27534E-01	7.46159E-00	1.27671E-03
11	1.30477E+03	1.14639E-02	2.45076E-07	5.85466E-01	8.04706E-00	1.04849E-03
12	1.34392E+03	1.28078E-02	2.37093E-07	5.66396E-01	8.61345E-00	1.1995F-03
13	1.38423E+03	1.41920E-02	2.30129E-07	5.49737E-01	9.16319E-00	1.05888E
14	1.42576E+03	1.56178E-02	2.23973E-07	5.25054E-01	9.25054E-00	1.00058E
15	1.46653E+03	1.70863E-02	2.18516E-07	5.22015E-01	1.02203E-01	9.47761E-03
16	1.51259E+03	1.85998E-02	2.13639E-07	5.10345E-01	1.07306E-01	8.99620E-03
17	1.55797E+03	2.01569E-02	2.09257E-07	4.99898E-01	1.12305E-01	8.55504E-03
18	1.60671E+03	2.17616E-02	2.05302E-07	4.90450E-01	1.17216E-01	8.14895E-03
19	1.65285E+03	2.34146E-02	2.01718E-07	4.81857E-01	1.22029E-01	7.77341E-03
20	1.70243E+03	2.51169E-02	1.98457E-07	4.74099E-01	1.26770E-01	7.42502E-03
21	1.75351E+03	2.68704E-02	1.95492E-07	4.66991E-01	1.31439E-01	7.10669E-03
22	1.80611E+03	2.86765E-02	1.92760E-07	4.60497E-01	1.36044E-01	6.79786E-03
23	1.86029E+03	3.05368E-02	1.90262E-07	4.54520E-01	1.40590E-01	6.51435E-03
24	1.91610E+03	3.24529E-02	1.87966E-07	4.49035E-01	1.45080E-01	6.24828E-03
25	1.97359E+03	3.44265E-02	1.85851E-07	4.43983E-01	1.49520E-01	5.99804E-03
26	2.03279E+03	3.64559E-02	1.83900E-07	4.39322E-01	1.53913E-01	5.76220E-03
27	2.09378E+03	3.85530E-02	1.82098E-07	4.35016E-01	1.58263E-01	5.53955E-03
28	2.15659E+03	4.07096E-02	1.80431E-07	4.31035E-01	1.62573E-01	5.32899E-03
29	2.22129E+03	4.29309E-02	1.79889E-07	4.27351E-01	1.66847E-01	5.12955E-03
30	2.28793E+03	4.52189E-02	1.77462F-07	4.23941E-01	1.71086E-01	4.94041E-03
31	2.35657E+03	4.75754E-02	1.76140E-07	4.20784E-01	1.75294E-01	4.76080E-03
32	2.42726E+03	5.00027E-02	1.74917E-07	4.17862E-01	1.79473E-01	4.59004E-03
33	2.50008E+03	5.25028E-02	1.73786E-07	4.15160E-01	1.83624E-01	4.42752E-03
34	2.57508E+03	5.59777E-02	1.72740E-07	4.12661E-01	1.87751E-01	4.27720E-03
35	2.65234E+03	5.77302E-02	1.71775E-07	4.10355E-01	1.91855E-01	4.12507E-03
36	2.73191E+03	6.04621E-02	1.70895E-07	4.08230E-01	1.95937E-01	3.98418E-03
37	2.81386E+03	6.32759E-02	1.70067E-07	4.06276E-01	2.00000E-01	3.84962F-03
38	2.89828E+03	6.61742E-02	1.69317E-07	4.04493E-01	2.04045E-01	3.72100E-03
39	2.98523E+03	6.91594E-02	1.68630E-07	4.02844E-01	2.08073E-01	3.59799E-03
40	3.07478E+03	7.22342E-02	1.68005E-07	4.01350E-01	2.12086E-01	3.48023E-03
41	3.16733E+03	7.54013E-02	1.67438E-07	3.99995E-01	2.16086E-01	3.31976E-03
42	3.26204E+03	7.86633E-02	1.66926E-07	3.98772E-01	2.20074E-01	3.25939E-03
43	3.35490E+03	8.20232E-02	1.66467E-07	3.97675E-01	2.24051E-01	3.15574E-03
44	3.46070E+03	8.54839E-02	1.66058E-07	3.96698E-01	2.28018E-01	3.05630E-03
45	3.56452E+03	8.90484E-02	1.65697E-07	3.95836E-01	2.31976E-01	2.96083E-03
46	3.67145E+03	9.27199E-02	1.65382E-07	3.95083E-01	2.35927E-01	2.86413E-03
47	3.78160E+03	9.65015E-02	1.65119E-07	3.94435E-01	2.39871E-01	2.78099E-03
48	3.89504E+03	1.00397E-01	1.64881E-07	3.93896E-01	2.43810E-01	2.69623E-03
49	4.01190E+03	1.04408E-01	1.64690E-07	3.93431E-01	2.47745E-01	2.61468E-03
50	4.13225E+03	1.08541E-01	1.64539E-07	3.93067E-01	2.51675E-01	2.53617E-03

*** TEST PROFILE NO. 2 *** TWO BLACK BODY SPECTRUM ***

J	DX	X	ERGS	CAL	SUM F.4L	ERG/SIGH	VELOCITY	?CNE MASS	J
51	4.25622E-03	1.12797E-01	3.92786E-01	2.55603E 01	2.46055E 04	6.92276E-03	0	6.89921E-03	52
52	4.38391E-03	1.17181E-01	3.92586E-01	2.59529E 01	2.39765E 09	6.89921E-03	0	7.05921E-04	53
53	4.51542E-03	1.21596E-01	3.92460E-01	2.63454E 01	2.31738E 09	7.39189E-03	0	7.39189E-03	54
54	4.65039E-03	1.26347E-01	3.92404E-01	2.67378E 01	2.24956E 09	7.52095E-03	0	7.52095E-03	55
55	4.79041E-03	1.31137E-01	3.92412E-01	2.71302E 01	2.18459E 09	7.65217E-03	0	7.65217E-03	56
56	4.93412E-03	1.36072E-01	3.92492E-01	2.75227E 01	2.12093E 09	7.74659E-03	0	7.74659E-03	57
57	5.08215E-03	1.41154E-01	3.92611E-01	2.79153E 01	2.05970E 09	7.97997E-03	0	7.97997E-03	58
58	5.23461E-03	1.46388E-01	3.92770E-01	2.83080E 01	2.00057E 09	8.21834E-03	0	8.21834E-03	59
59	5.39165E-03	1.51780E-01	3.92930E-01	2.87010E 01	1.94334E 09	8.46489E-03	0	8.46489E-03	60
60	5.55340E-03	1.57333E-01	3.93227E-01	2.90942E 01	1.88792E 09	8.71884E-03	0	8.71884E-03	61
61	5.72000E-03	1.63053E-01	3.93503E-01	2.94877E 01	1.83422E 09	9.04040E-03	0	9.04040E-03	62
62	5.89160E-03	1.68945E-01	3.94802E-01	2.98815E 01	1.78215E 09	9.42982E-03	0	9.42982E-03	63
63	6.06835E-03	1.75013E-01	3.94118E-01	3.02757E 01	1.73163E 09	9.52731E-03	0	9.52731E-03	64
64	6.25040E-03	1.81264E-01	3.94444E-01	3.06701E 01	1.68258E 09	9.81123E-03	0	9.81123E-03	65
65	6.43791E-03	1.87702E-01	3.94720E-01	3.10649E 01	1.63493E 09	1.01075E-02	0	1.01075E-02	66
66	6.63105E-03	1.94333E-01	3.95095E-01	3.14600E 01	1.58861E 09	1.0410RE-02	0	1.0410RE-02	67
67	6.62998E-03	2.01163E-01	3.95406E-01	3.18554E 01	1.54356E 09	1.07231E-02	0	1.07231E-02	68
68	7.03488E-03	2.08198E-01	3.95698E-01	3.22511E 01	1.49971E 09	1.12446E-02	0	1.12446E-02	69
69	7.24593E-03	2.15444E-01	3.95963E-01	3.26470E 01	1.45700E 09	1.17717E-02	0	1.17717E-02	70
70	7.46331E-03	2.22907E-01	3.96193E-01	3.30432E 01	1.41539E 09	1.23689E-02	0	1.23689E-02	71
71	7.68721E-03	2.30594E-01	3.96389E-01	3.34396E 01	1.37481E 09	1.29693E-02	0	1.29693E-02	72
72	7.91782E-03	2.38512E-01	3.96519E-01	3.38361E 01	1.33524E 09	1.34710E-02	0	1.34710E-02	73
73	8.15536E-03	2.46667E-01	3.96600E-01	3.42327E 01	1.29661E 09	1.39039E-02	0	1.39039E-02	74
74	8.40002E-03	2.55067E-01	3.96615E-01	3.46293E 01	1.25889E 09	1.41680E-02	0	1.41680E-02	75
75	8.65202E-03	2.63719E-01	3.96557E-01	3.50259E 01	1.22205E 09	1.45937E-02	0	1.45937E-02	76
76	8.91156E-03	2.72631E-01	3.96429E-01	3.54223E 01	1.18604E 09	1.49912E-02	0	1.49912E-02	77
77	9.17933E-03	2.81810E-01	3.96151E-01	3.58185E 01	1.15019E 09	1.44109E-02	0	1.44109E-02	78
78	9.45429E-03	2.91264E-01	3.95817E-01	3.62144E 01	1.11643E 09	1.49432E-02	0	1.49432E-02	79
79	9.73792E-03	3.01002E-01	3.95539E-01	3.66098E 01	1.08276E 09	1.52885E-02	0	1.52885E-02	80
80	1.00301E-02	3.11032E-01	3.95319E-01	3.70048E 01	1.04983E 09	1.57472E-02	0	1.57472E-02	81
81	1.03310E-02	3.21363E-01	3.94294E-01	3.73991E 01	1.01760E 09	1.62196E-02	0	1.62196E-02	81
82	1.06409E-02	3.32004E-01	3.94174E-01	3.77923E 01	9.86072E 08	1.67062E-02	0	1.67062E-02	82
83	1.09601E-02	3.42964E-01	3.94367E-01	3.92659E-01	9.55213E 08	1.72074E-02	0	1.72074E-02	83
84	1.12889E-02	3.54253E-01	3.94394E-01	3.91653E-01	9.25014E 08	1.77236E-02	0	1.77236E-02	84
85	1.16276E-02	3.65981E-01	3.93470E-01	3.90515E-01	8.95463E 08	1.82553E-02	0	1.82553E-02	85
86	1.19764E-02	3.77857E-01	3.892937E-01	3.89242E-01	8.56549E 08	1.88070E-02	0	1.88070E-02	86
87	1.23357E-02	3.90193E-01	3.82347E-01	3.87832E-01	8.38262E 08	1.93471E-02	0	1.93471E-02	87
88	1.27058E-02	4.02898E-01	3.81698E-01	3.86282E-01	8.10594E 08	1.99481E-02	0	1.99481E-02	88
89	1.30870E-02	4.15985E-01	3.80990E-01	3.84591E-01	7.83538E 08	2.05465E-02	0	2.05465E-02	89
90	1.34796E-02	4.29465E-01	3.80222E-01	3.82757E-01	7.57089E 08	2.11629E-02	0	2.11629E-02	90
91	1.38839E-02	4.4349E-01	3.7935E-01	3.80780E-01	7.31242E 08	2.17979E-02	0	2.17979E-02	91
92	1.42005E-02	4.57649E-01	3.78503E-01	3.80861E-01	7.05992E 08	2.24517E-02	0	2.24517E-02	92
93	1.47295E-02	4.72379E-01	3.757561E-01	3.76400E-01	6.83354E 08	2.30277E-02	0	2.30277E-02	93
94	1.51714E-02	4.87550E-01	3.73990E-01	4.05154E-01	6.57271E 08	2.38192E-02	0	2.38192E-02	94
95	1.56265E-02	5.03177E-01	3.55492E-01	4.24080E-01	6.32779E 08	2.45336E-02	0	2.45336E-02	95
96	1.60933E-02	5.19272E-01	3.54372E-01	4.31482E-01	6.10902E 08	2.52656E-02	0	2.52656E-02	96
97	1.65782E-02	5.35850E-01	3.53196E-01	4.20340E-01	5.88588E 08	2.60277E-02	0	2.60277E-02	97
98	1.70755E-02	5.52926E-01	3.51966E-01	4.05154E-01	5.66855E 08	2.68095E-02	0	2.68095E-02	98
99	1.75878E-02	5.70513E-01	3.50653E-01	4.02272E-01	5.45700E 08	2.74129E-02	0	2.74129E-02	99
100	1.81154E-02	5.88629E-01	3.49353E-01	4.05940E-01	5.25117E 08	2.84412E-02	0	2.84412E-02	100

*** TEST PROBLEM NO. 2 *** TWO BLACK BODY SPECTRUM ***

J	Dx	x	ERGS	CAL	SUM CAL	FRGSM	VFRGSM	VFRGSM	VMNE MASS	J
101	1.86589E-02	6.07288E-01	1.67967E 0.7	3.53461E-01	4.49475E 0.1	5.05103E 0.8	2.97944E-02	1.01		
102	1.92186E-02	6.26506E-01	1.46538E 0.7	3.50066E-01	4.52975E 0.1	4.95654E 0.8	3.01733E-02	1.02		
103	1.97952E-02	6.46302E-01	1.45063E 0.7	3.46544E-01	4.56441E 0.1	4.66765E 0.8	3.10784E-02	1.03		
104	2.03899E-02	6.66691E-01	1.43547E 0.7	3.42321E-01	4.59879E 0.1	4.48437E 0.8	3.20108E-02	1.04		
105	2.10007E-02	6.87691E-01	1.41990E 0.7	3.39702E-01	4.63262E 0.1	4.30649E 0.8	3.29711E-02	1.05		
106	2.16307E-02	7.09322E-01	1.40395E 0.7	3.35392E-01	4.66616E 0.1	4.13413E 0.8	3.36603E-02	1.06		
107	2.22797E-02	7.31602E-01	1.38745E 0.7	3.31497E-01	4.69931E 0.1	3.96707E 0.8	3.49791E-02	1.07		
108	2.29481E-02	7.54550E-01	1.37101E 0.7	3.27522E-01	4.73206E 0.1	3.80535E 0.8	3.63234E-02	1.08		
109	2.36365E-02	7.78186E-01	1.35476E 0.7	3.23473E-01	4.75441E 0.1	3.64894E 0.8	3.71993E-02	1.09		
110	2.43456E-02	8.02532E-01	1.33683E 0.7	3.19356E-01	4.79614E 0.1	3.49744E 0.8	3.82226E-02	1.10		

CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
-5.6009E-12	4.7198E-10	7.9497E-11	100	2	8.7225E 08	1.0000E-03	-8.6107E-02	8.1221E-02	-4.8853E-01
25	7.0711E-11	-1.5230E-01	1.4749E-01	-4.0932E-08	0	0	0	0	110
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
DTPP	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
50	7.1041E-09	3.0000E-10	109	3	8.8265E 09	2.0375E-03	4.2791E 00	2.0560E 01	2.4839E 01
2.8142E-09	4.8480E-10	1.1354E-01	-3.1435E 01	3.1430E 01	-9.8675E-05	0	0	0	110
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
DTPP	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
75	1.4604E-08	3.0000E-10	109	5	1.4918E 10	4.2177E-03	3.7882E 01	7.6222E 01	1.1410E 02
7.6489E-09	2.5394E-09	2.3344E 01	-1.1286E 02	1.1285E 02	-3.9257E-04	0	0	0	110
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
DTPP	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
100	2.2104E-08	3.0000E-10	109	7	1.9476E 10	6.5430E-03	7.1662E 01	1.5437E 02	2.2603E 02
1.1606E-08	3.6794E-09	3.5333E 01	-2.2049E 02	2.2049E 02	-8.0308E-04	0	0	0	110
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
DTPP	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
125	2.9604E-08	3.0000E-10	109	9	2.3100E 10	9.0175E-03	1.0779E 02	2.4748E 02	3.5527E 02
1.5380E-08	4.66664E-09	4.7323E 01	-3.5421E 02	3.5420E 02	-1.3023E-03	0	0	0	110
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
DTPP	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
150	7.6735E-08	2.3019E-09	109	19	1.7129E 10	2.3932E-02	2.8225E 02	6.6286E 02	9.4572E 02
5.5212E-08	1.6513E-08	4.7806E 01	-9.3875E 02	9.3875E 02	-4.0210E-03	0	0	0	110
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
DTPP	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
175	1.4503E-07	3.2275E-09	109	29	1.4295E 10	4.3950E-02	4.2203E 02	1.0018E 03	1.4239E 03
9.9604E-08	2.9522E-08	4.7809E 01	-1.4108E 03	1.4108E 03	-7.0607E-03	0	0	0	110
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
DTPP	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
200	2.1357E-07	2.6840E-09	109	37	1.2745E 10	6.4627E-02	5.4078E 02	1.2019E 03	1.7487E 03
1.3721E-07	4.2902E-08	4.7809E 01	-1.7455E 03	1.7455E 03	-9.4889E-03	0	0	0	110
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
DTPP	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
225	2.8084E-07	2.6931E-09	109	43	1.1775E 10	8.3684E-02	6.3273E 02	1.3615E 03	1.9942E 03
1.6935E-07	5.3733E-08	4.7809E 01	-1.9913E 03	1.9913E 03	-1.1493E-02	0	0	0	110
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MVPULSE	MVPREC	MOMENTUM
DTPP	DTPPS	ETOTAL	ENVNEG	ENVPOS	L-BOUND	X(JBND1)	X(JBND2)	R-BOUND	JFIN
250	3.3887E-07	1.0487E-09	109	50	1.1039E 10	1.0232E-01	7.0695E 02	1.6471E 03	2.1941E 03
1.9875E-07	6.4040E-08	4.7809E 01	-2.1919E 03	2.1919E 03	-1.3114E-02	0	0	0	110

CYCLE	TIME	DTNH		JSTAR		JPMAX		XJPMAX		WYPREC		
		DTPP	DTPULS	ETOTAL	ENVNEG	EMVPOS	L-BOUND	X(JBND1)	X(JBND2)	2-BOUND	2-BOUND	
2.2331E-07	4.1437E-07	2.9713E-09	1.09	52	1.0380E-10	1.1943E-01	7.6716E-02	1.5227E-02	1.5227E-02	2.3609E-02	2.3609E-02	
2.5460E-07	7.1978E-08	4.7809E-01	-2.3625E-03	2.3625E-03	-1.4611E-02	0	0	0	0	2.7314E-01	1.10	
2.8155E-07	8.2870E-08	4.7809E-01	-2.6153E-01	2.6153E-01	-1.5869E-02	0	0	0	0	0	0	
3.0583E-07	1.0608E-07	2.6523E-07	2.6523E-09	1.09	56	9.9014E-09	1.3850E-01	3.2952E-02	1.7004E-03	2.5204E-03	2.5204E-03	
3.3142E-07	1.1822E-07	4.7809E-01	-2.7763E-03	2.6554E-03	-1.7073E-02	0	0	0	0	0	0	
3.6091E-07	1.3777E-07	2.6368E-07	2.8794E-09	1.09	63	9.0781E-09	1.7773E-01	9.6300E-02	1.324E-02	2.7764E-02	2.7764E-02	
4.0077E-07	4.7808E-01	-2.8870E-03	2.8970E-03	-1.8967E-02	0	0	0	0	0	0	0	
4.4213E-07	8.2528E-07	2.7194E-09	1.09	66	8.7178E-09	1.9713E-01	1.0306E-03	1.2528E-03	2.8992E-03	2.8992E-03	2.8992E-03	
4.8422E-07	7.5661E-07	2.8794E-07	4.7808E-01	-2.9819E-03	2.9819E-03	-1.9742E-02	0	0	0	0	0	
5.2631E-07	1.3594E-07	2.8794E-07	4.7808E-01	-3.0796E-03	3.0796E-03	-2.0504E-02	0	0	0	0	0	
5.7133E-07	4.42	3.7902E-07	1.3777E-07	2.7194E-09	1.09	71	8.1350E-09	2.3379E-01	1.1275E-03	1.4691E-03	2.9956E-03	2.9956E-03
6.2544E-07	4.42	8.7133E-07	2.8330E-09	1.09	73	7.8481E-09	2.4977E-01	1.2110E-03	1.6243F-03	3.1453E-03	3.1453E-03	3.1453E-03
6.8155E-07	4.42	4.0077E-07	4.5430E-07	4.7808E-01	-3.1326E-03	3.1326E-03	-2.06889E-02	0	0	0	0	0
7.4276E-07	4.42	5.7133E-07	4.42	4.7808E-01	122	90	0	0	0	0	0	0
8.0497E-07	4.42	6.7133E-07	4.7982E-07	4.7808E-01	-3.0958E-03	3.0926E-03	-2.0889E-02	0	0	0	0	0
8.7118E-07	4.42	8.7133E-07	2.8330E-09	90	41	7.8481E-09	2.4977E-01	9.4477E-02	2.1774E-02	3.1721E-02	3.1721E-02	3.1721E-02
9.4244E-07	4.42	9.7133E-07	4.2038E-07	4.7808E-01	-3.1135E-03	3.1135E-03	-2.0974E-02	0	0	0	0	0
10.1371E-07	4.42	1.07133E-07	4.1275E-07	4.7808E-01	122	90	0	0	0	0	0	0

0.798E-07 445 -12 102

CYCLE	TIME	DTIME	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
DTPP	DTPULS	ETOTAL	ENVNEG	ENVPOS	L-ROUND	XIJANDI1	XIJANDI21	S-ROUND	JFIN
445	8.7953E-07	2.7230E-09	102	41	7.9026E-09	2.4991E-01	8.9102E-02	2.278AE-03	3.1199F-03
3.9479E-07	1.1275E-07	4.7794E-01	-3.1135E-03	3.1132E-03	-2.0974E-02	0	0	9.2401E-01	103

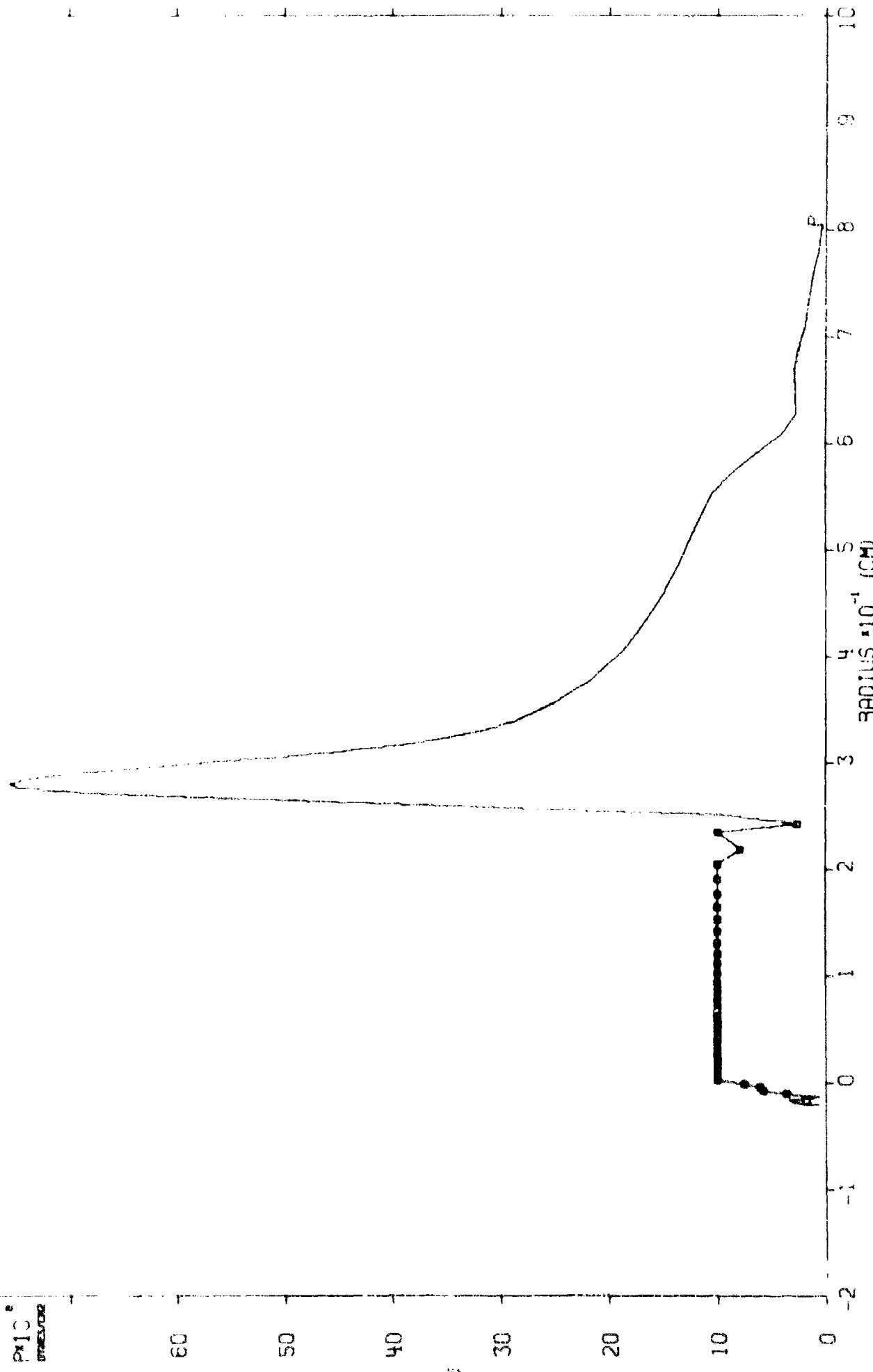
CYCLE	TIME	DTIME	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
DTPP	DTPULS	ETOTAL	ENVNEG	ENVPOS	L-ROUND	XIJANDI1	XIJANDI21	R-ROUND	JFIN
450	8.9318E-07	2.6519E-09	102	41	7.7934E-09	2.5013E-01	8.3551E-02	2.3142E-03	3.1409F-03
4.0416E-07	1.0722E-07	4.7794E-01	-3.1327E-03	3.1294E-03	-2.1978E-02	0	0	9.3404E-01	103

CYCLE	TIME	DTIME	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
DTPP	DTPULS	ETOTAL	ENVNEG	ENVPOS	L-ROUND	XIJANDI1	XIJANDI21	R-ROUND	JFIN
475	9.6413E-07	2.7656E-09	102	46	7.6499E-09	2.7166E-01	9.3657E-02	2.2970E-03	3.2335F-03
4.2269E-07	1.2243E-07	4.7801E-01	-3.2279E-03	3.2246E-03	-2.1727E-02	0	0	8.3619E-01	103

CYCLE TIME DTIME JSTAR JPMAX PMAX XJPMAX MYPULSE MYPREC MOMENTUM

DTPP	DTPULS	ETOTAL	ENVNEG	ENVPOS	L-ROUND	XIJANDI1	XIJANDI21	R-ROUND	JFIN
488	1.0002E-06	3.02228E-09	102	49	7.5793E-09	2.8081E-01	9.4767E-02	2.3251E-03	3.272RF-03
4.3101E-07	1.2503E-07	4.7804E-01	-3.2664E-03	3.2631E-03	-2.2017E-02	0	0	8.34274E-01	103

TEST PROBLEM NO. 2 ■■■ TBC BLACK BODY SPECTRUM ■■■
 $\tau_{\text{out}} = 195$ $\tau_{\text{in}} = 1.00010$



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APPENDIX V

TEST PROBLEM 3

(F PUFF)

12	CUSPI(2) 6.33+9	CUSPA(2) .006	CUSPC(2) .75+12	CUSPD(2) .3096+12	CUSPG(2) 1.59	CUSPS(2) 0.		
11	RHO(2) 2.78	EQSTC(2) 1.04833+12	EQSTD(2) 0.0	EQSTE(2) 1.17+11	EQSTG(2) 1.59	EQSTH(2) 20	EQSTS(2) 0.0	PMIN(2) -1.+10
10	MATL(2) MATL 2							
9	CUSPI(1) 6.33+9	CUSPA(1) .006	CUSPC(1) .75+12	CUSPD(1) .3096+12	CUSPG(1) 1.59	CUSPS(1) 0.		
8	RHO(1) 2.78	EQSTC(1) 1.04833+12	EQSTD(1) 0.0	EQSTE(1) 1.17+11	EQSTG(1) 1.59	EQSTH(1) 20	EQSTS(1) 0.0	PMIN(1) -1.+10
7	MATL(1) MATL 1							

6	DX 22-2	TIME 1-12	RZ(1) 1.0	RZ(2) 1.04	RZ(3) #51	RZ(4) 1.0		
5	JFIN 201	NZ(1) 100	NZ(2) 160	NZ(3) 161	NZ(4) 200			
4	JBND(1) 101	JBND(2) 169						
3	UFACE .5	UZERO 1.79+4	UFIN2 101.					
2	NRZC 4	NMTR_S 3	JRZL 20	JZPUL 40	NPRIN 50	NTAPE 25	NJEDIT 0	NTEDT 0
1	DISCPT(I), I = 1, 10 *** TEST PROBLEM NO. 3 *** TWO-WAVE EQUATION OF STATE *** PLATE SLAP							

17	JCYCS 600	NTEST 30						
16	CKP 20	TS 2.4-6						
15	CUSPI(3) 0.	CUSPA(3) 0	CUSPC(3) 0	CUSPD(3) 0	CUSPG(3) 0	CUSPS(3) 0		
14	RHD(3) 2.65	EQSTC(3) 8.6+11	EQSTD(3) -2.232+11	EQSTE(3) 8.87+10	EQSTG(3) .621	EQSTH(3) 25	EQSTS(3) 0.0	PMYN(3) -4. +09
13	MATL(3) MATL 3							

INPUT PARAMETERS FOR -

** TEST PROBLEM NO. 3 ** TWO-WAVE EQUATION OF STATE ** PLATE SLAP
*** THIS PROBLEM WAS RUN ON P-PURE/1624 ***

NRFLC	NMFLS	JRFL	JZFL	NPFLN	NPFLN < 300E-01	UPERD	JFIN2
4	3	20	40	50	1.79CE-01	1.79CE-04	101

LOADING CONSTANTS

RATIO 1-000E-00 TO ZONE	100
RATIO 1-005E-00 TO ZONE	160
RATIO 4-51CE-01 TO ZONE	161
RATIO 1-000E-00 TO ZONE	200

JFIN	JCYCS	NTEST	NTAPE	CAP	TIME
201	600	30	25	2.00E-30	2.400E-96 1.000E-12

MATERIAL PROPERTIES FOR MATT L
MATERIAL THICKNESS = 2.200E-01

101 = 100 + 1

*** TEST PROBLEM NO. 3 *** TWO-WAVE EQUATION ONE STATE *** PLATE SLAP

J	X	VELOCITY	ZONE MASS
1	0	1.79000E 04	0
2	2.20000E-03	1.79000E 04	6.11600E-03
3	4.40000E-03	1.79000E 04	6.11600E-03
4	6.60000E-03	1.79000E 04	6.11600E-03
5	8.80000E-03	1.79000E 04	6.11600E-03
6	1.10000E-02	1.79000E 04	6.11600E-03
7	1.32000E-02	1.79000E 04	6.11600E-03
8	1.54000E-02	1.79000E 04	6.11600E-03
9	1.76000E-02	1.79000E 04	6.11600E-03
10	1.98000E-02	1.79000E 04	5.11600E-03
11	2.20000E-02	1.79000E 04	6.11600E-03
12	2.42000E-02	1.79000E 04	6.11600E-03
13	2.64000E-02	1.79000E 04	4.11620E-02
14	2.86000E-02	1.79000E 04	6.11620E-03
15	3.08000E-02	1.79000E 04	6.11620E-03
16	3.30000E-02	1.79000E 04	6.11600E-03
17	3.52000E-02	1.79000E 04	6.11600E-03
18	3.74000E-02	1.79000E 04	6.11600E-03
19	3.96000E-02	1.79000E 04	6.11620E-03
20	4.18000E-02	1.79000E 04	6.11620E-03
21	4.40000E-02	1.79000E 04	6.11600E-03
22	4.62000E-02	1.79000E 04	6.11600E-03
23	4.84000E-02	1.79000E 04	6.11600E-03
24	5.06000E-02	1.79000E 04	6.11600E-03
25	5.28000E-02	1.79000E 04	6.11620E-03
26	5.50000E-02	1.79000E 04	6.11600E-03
27	5.72000E-02	1.79000E 04	6.11600E-03
28	5.94000E-02	1.79000E 04	6.11600E-03
29	6.16000E-02	1.79000E 04	6.11600E-03
30	6.38000E-02	1.79000E 04	6.11600E-03
31	6.60000E-02	1.79000E 04	6.11600E-03
32	6.82000E-02	1.79000E 04	6.11600E-03
33	7.04000E-02	1.79000E 04	6.11600E-03
34	7.26000E-02	1.79000E 04	6.11600E-03
35	7.48000E-02	1.79000E 04	6.11600E-03
36	7.70000E-02	1.79000E 04	6.11600E-03
37	7.92000E-02	1.79000E 04	6.11600E-03
38	8.14000E-02	1.79000E 04	6.11600E-03
39	8.36000E-02	1.79000E 04	6.11600E-03
40	8.58000E-02	1.79000E 04	6.11600E-03
41	8.80000E-02	1.79000E 04	6.11600E-03
42	9.02000E-02	1.79000E 04	6.11600E-03
43	9.24000E-02	1.79000E 04	6.11600E-03
44	9.46000E-02	1.79000E 04	6.11600E-03
45	9.68000E-02	1.79000E 04	5.11600E-03
46	9.90000E-02	1.79000E 04	6.11600E-03
47	1.01200E-01	1.79000E 04	6.11600E-03
48	1.03400E-01	1.79000E 04	6.11600E-03
49	1.05600E-01	1.79000E 04	6.11620E-03
50	1.07800E-01	1.79000E 04	6.11670E-03

*** TEST PROBLEM NO. 3 *** TWO-WAVE EQUATION OF STATE *** PLATE SLAP

J	X	VELOCITY	ZONE	MASS
51	1.10000E-01	1.79020E 04	6.11600E-03	6.11600E-03
52	1.12200E-01	1.79000E 04	6.11600E-03	6.11600E-03
53	1.14400E-01	1.79000E 04	6.11600E-03	6.11600E-03
54	1.16600E-01	1.79000E 04	6.11600E-03	6.11600E-03
55	1.18800E-01	1.79000E 04	6.11600E-03	6.11600E-03
56	1.21000E-01	1.79000E 04	6.11600E-03	6.11600E-03
57	1.23200E-01	1.79000E 04	6.11600E-03	6.11600E-03
58	1.25400E-01	1.79000E 04	6.11600E-03	6.11600E-03
59	1.27600E-01	1.79000E 04	6.11600E-03	6.11600E-03
60	1.29800E-01	1.79000E 04	6.11600E-03	6.11600E-03
61	1.32000E-01	1.79000E 04	6.11600E-03	6.11600E-03
62	1.34200E-01	1.79000E 04	6.11600E-03	6.11600E-03
63	1.36400E-01	1.79000E 04	6.11600E-03	6.11600E-03
64	1.38600E-01	1.79000E 04	6.11600E-03	6.11600E-03
65	1.40800E-01	1.79000E 04	6.11600E-03	6.11600E-03
66	1.43000E-01	1.79000E 04	6.11600E-03	6.11600E-03
67	1.45200E-01	1.79000E 04	6.11600E-03	6.11600E-03
68	1.47400E-01	1.79000E 04	6.11600E-03	6.11600E-03
69	1.49600E-01	1.79000E 04	6.11600E-03	6.11600E-03
70	1.51800E-01	1.79000E 04	6.11600E-03	6.11600E-03
71	1.54000E-01	1.79000E 04	6.11600E-03	6.11600E-03
72	1.56200E-01	1.79000E 04	6.11600E-03	6.11600E-03
73	1.58400E-01	1.79000E 04	6.11600E-03	6.11600E-03
74	1.60600E-01	1.79000E 04	6.11600E-03	6.11600E-03
75	1.62800E-01	1.79000E 04	6.11600E-03	6.11600E-03
76	1.65000E-01	1.79000E 04	6.11600E-03	6.11600E-03
77	1.67200E-01	1.79000E 04	6.11600E-03	6.11600E-03
78	1.69400E-01	1.79000E 04	6.11600E-03	6.11600E-03
79	1.71600E-01	1.79000E 04	6.11600E-03	6.11600E-03
80	1.73800E-01	1.79000E 04	6.11600E-03	6.11600E-03
81	1.76000E-01	1.79000E 04	6.11600E-03	6.11600E-03
82	1.78200E-01	1.79000E 04	6.11600E-03	6.11600E-03
83	1.80400E-01	1.79000E 04	6.11600E-03	6.11600E-03
84	1.82600E-01	1.79000E 04	6.11600E-03	6.11600E-03
85	1.84800E-01	1.79000E 04	6.11600E-03	6.11600E-03
86	1.87000E-01	1.79000E 04	6.11600E-03	6.11600E-03
87	1.89200E-01	1.79000E 04	6.11600E-03	6.11600E-03
88	1.91400E-01	1.79000E 04	6.11600E-03	6.11600E-03
89	1.93600E-01	1.79000E 04	6.11600E-03	6.11600E-03
90	1.95800E-01	1.79000E 04	6.11600E-03	6.11600E-03
91	1.98000E-01	1.79000E 04	6.11600E-03	6.11600E-03
92	2.00200E-01	1.79000E 04	6.11600E-03	6.11600E-03
93	2.02400E-01	1.79000E 04	6.11600E-03	6.11600E-03
94	2.04600E-01	1.79000E 04	6.11600E-03	6.11600E-03
95	2.06800E-01	1.79000E 04	6.11600E-03	6.11600E-03
96	2.09000E-01	1.79000E 04	6.11600E-03	6.11600E-03
97	2.11200E-01	1.79000E 04	6.11600E-03	6.11600E-03
98	2.13400E-01	1.79000E 04	6.11600E-03	6.11600E-03
99	2.15600E-01	1.79000E 04	6.11600E-03	6.11600E-03
100	2.17800E-01	1.79000E 04	6.11600E-03	6.11600E-03

*** TEST PROBLEM NO. 3 *** TWO-WAVE EQUATION OF STATE *** PLATE SLAB

J X VELOCITY ZONE MASS

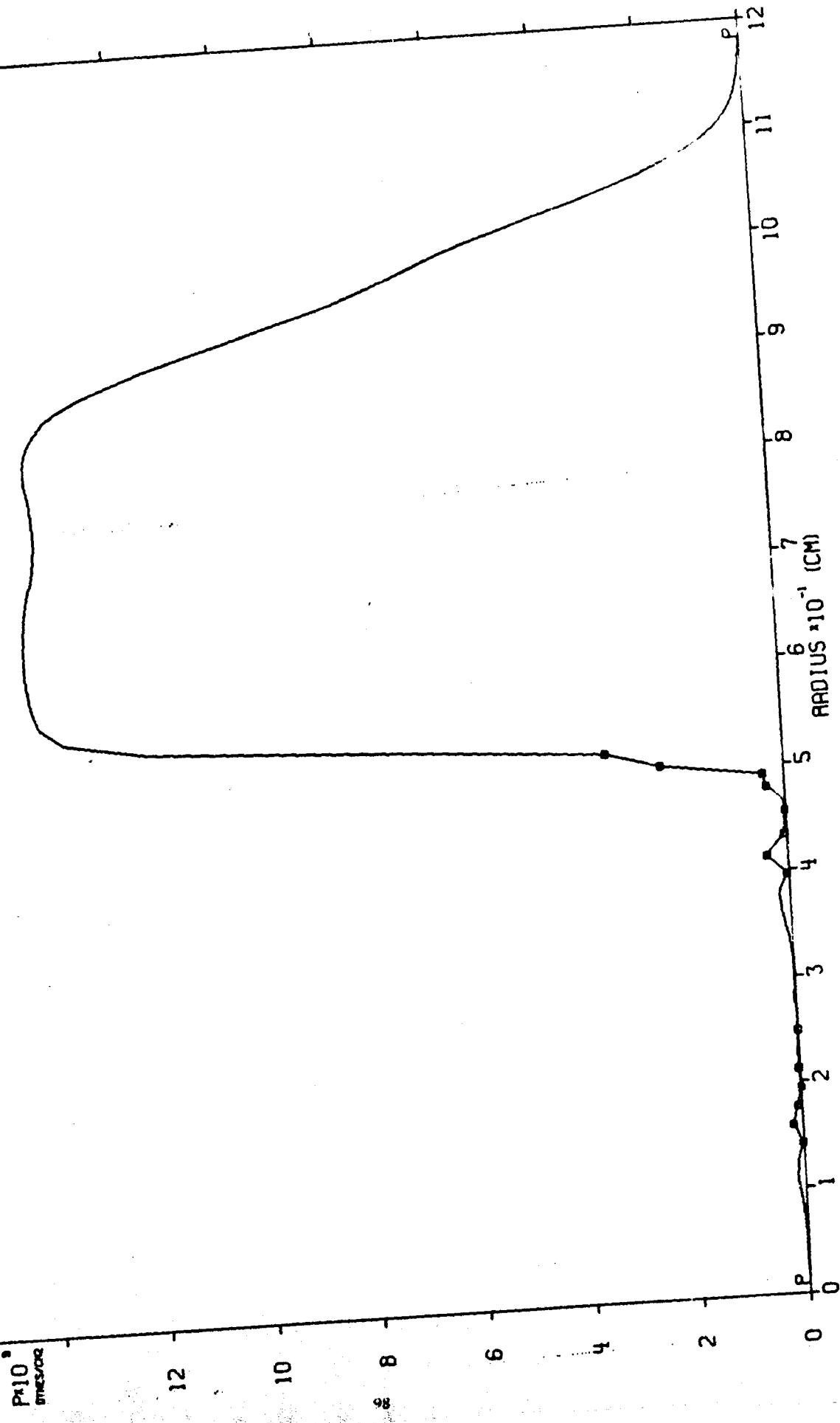
101	2.23000E-01	1.34250E 04	6.11160E-03
102	2.22288E-01	8.95000E 03	6.36064E-03
103	2.24668E-01	6.47500E 03	6.61507E-03
104	2.27142E-01	0	6.87967E-03

CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
25	4.7198E-10	7.9497E-11	JSTAR 106 ENVNEG 0	101 EMVPNS 0	9.9088E 03 1-BOUND	2.2001E-01 X(JBND1)	1.1065E 04 X(JBND1)	1.1381E-02 R-ROUND	1.1065E 04 JFIN 201
	DTPP	DTIPULS	ETOTAL						
1.1167E-05	1.1167E-05	2.3488E 00							
CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
50	2.5444E-08	1.8651E-09	JSTAR 114 ENVNEG 0	103 EMVPNS 0	1.4186E 10 L-BOUND	2.2486E-01 X(JBND1)	1.0974E 04 X(JBND1)	9.0577E 02 R-ROUND	1.1065E 04 JFIN 201
	DTPP	DTIPULS	ETOTAL						
7.3000E-07	7.7362E-07	2.3528E 00							
CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
51	2.7309E-08	1.8670E-09	JSTAR 115 ENVNEG 0	103 EMVPNS 0	1.4187E 10 L-BJND	2.2487E-01 X(JBND1)	1.0954E 04 X(JBND1)	1.1114E 02 R-ROUND	1.1065E 04 JFIN 201
	DTPP	DTIPULS	ETOTAL						
7.7991E-07	7.7207E-07	2.3528E 00							
CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
51	2.7309E-08	1.8670E-09	JSTAR 69 ENVNEG 0	57 EMVPNS 0	1.4187F 10 L-BOUND	2.2487F-01 X(JBND1)	1.0954E 04 X(JBND1)	1.1114E 02 R-ROUND	1.1065E 04 JFIN 155
	DTPP	DTIPULS	ETOTAL						
7.7991E-08	7.7207E-07	2.3526E 00							
CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
75	7.9672E-08	2.2119E-09	JSTAR 79 ENVNEG 0	59 EMVPNS 0	1.4425E 10 L-BOUND	2.3031E-01 X(JBND1)	1.0368E 04 X(JBND1)	6.9712E 02 R-ROUND	1.1065E 04 JFIN 155
	DTPP	DTIPULS	ETOTAL						
7.6707E-07	7.1674E-07	2.3529E 00							
CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
100	1.3684E-07	2.3944E-09	JSTAR 87 ENVNEG 0	69 EMVPNS 0	1.4349E 10 L-BOUND	2.6245E-01 X(JBND1)	1.0475E 04 X(JBND1)	5.9966E 02 R-ROUND	1.1065E 04 JFIN 155
	DTPP	DTIPULS	ETOTAL						
7.7114E-07	7.3005E-07	2.3532F 00							
CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
125	2.0342E-07	2.6569E-09	JSTAR 93 ENVNEG 0	77 EMVPNS 0	1.4298E 10 L-BOUND	2.9897E-01 X(JBND1)	1.0564E 04 X(JBND1)	5.0080E 02 R-ROUND	1.1065E 04 JFIN 155
	DTPP	DTIPULS	ETOTAL						
7.7305E-07	7.3888E-07	2.3536E 00							
CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
150	2.7330E-07	2.8567E-09	JSTAR 99 ENVNEG 0	83 EMVPNS 0	1.4264E 10 L-BOUND	3.3499E-01 X(JBND1)	1.0571E 04 X(JBND1)	4.9390E 02 R-ROUND	1.1065E 04 JFIN 155
	DTPP	DTIPULS	ETOTAL						
7.7574E-07	7.4111E-07	2.3536E 00							
CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
152	2.7823E-07	2.8667E-09	JSTAR 99 ENVNEG 0	83 EMVPNS 0	1.4261E 10 L-BOUND	3.3504E-01 X(JBND1)	1.0513E 04 X(JBND1)	5.5227E 02 R-ROUND	1.1065E 04 JFIN 155
	DTPP	DTIPULS	ETOTAL						
7.7588E-07	7.3714E-07	2.3535E 00							
	2.7922E-07	152	34	65					
CYCLE	TIME	DNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
152	2.7823E-07	2.8667E-09	JSTAR 65 ENVNEG 0	49 EMVPNS 0	1.4261E 10 L-BOUND	3.3504E-01 X(JBND1)	1.0513E 04 X(JBND1)	5.5227E 02 R-ROUND	1.1065E 04 JFIN 121
	DTPP	DTIPULS	ETOTAL						
7.7588E-07	7.3714E-07	2.3527E 00							

CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
175	3.2447E-07	1.9101E-09	EMVNEG	52	1.4237E-10	3.5651E-01	1.0455E-04	5.9945E-32	1.1061E-04
		DTPP	EMVPOS	52	1.-L-ROUND	XIJRN01	XIJRN021	P-BOUND	JFIN
7.7721E-07	7.3439E-07	ETOTAL		5.7980E-03	2.2294E-01		8.4902E-01	1.1820E-01	1.121
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
200	3.8108E-07	2.8654E-09	EMVNEG	71	1.4226E-10	1.3901E-01	4.2465E-03	5.8184E-33	1.1065E-04
		DTPP	EMVPOS	71	1.-L-ROUND	XIJRN01	XIJRN021	R-RGUND	JFIN
7.77179E-07	2.9850E-07	ETOTAL		6.5634E-03	2.2345E-01		8.4802E-01	1.1820E-01	1.121
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
225	4.3673E-07	2.8649E-09	EMVNEG	74	1.4219E-10	1.6549E-01	4.1142E-03	5.9520E-33	1.1065E-04
		DTPP	EMVPOS	74	1.-L-ROUND	XIJRN01	XIJRN021	R-RGUND	JFIN
7.7815E-07	2.8934E-07	ETOTAL		6.9449E-03	2.2394E-01		8.4902E-01	1.1820E-01	1.121
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
250	4.9869E-07	1.9111E-09	EMVNEG	77	1.4216E-10	2.0068E-01	3.8310E-03	7.2341E-33	1.1065E-04
		DTPP	EMVPOS	77	1.-L-ROUND	XIJRN01	XIJRN021	R-RGUND	JFIN
7.7836E-07	2.6949E-07	ETOTAL		6.9904E-03	2.2450E-01		8.4802E-01	1.1820E-01	1.121
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
275	5.5725E-07	2.86562E-09	EMVNEG	79	1.4213E-10	2.2961E-01	3.7275E-03	7.3439E-33	1.1071E-04
		DTPP	EMVPOS	79	1.-L-ROUND	XIJRN01	XIJRN021	R-RGUND	JFIN
7.7896E-07	2.6226E-07	ETOTAL		6.9879E-03	2.2502E-01		8.4902E-01	1.1820E-01	1.121
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
300	6.1329E-07	2.2931E-09	EMVNEG	82	1.4212E-10	2.5936E-01	3.9070E-03	7.1692E-33	1.1075E-04
		DTPP	EMVPOS	82	1.-L-ROUND	XIJRN01	XIJRN021	R-RGUND	JFIN
7.7936E-07	2.7491E-07	ETOTAL		6.9347E-03	2.2552E-01		8.4802E-01	1.1820E-01	1.121
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
325	6.7554E-07	2.86608E-09	EMVNEG	86	1.4208E-10	2.9313E-01	4.0541E-03	7.0240E-33	1.1082E-04
		DTPP	EMVPOS	86	1.-L-ROUND	XIJRN01	XIJRN021	R-RGUND	JFIN
7.7997E-07	2.8562E-07	ETOTAL		6.9914E-03	2.2608E-01		8.4802E-01	1.1820E-01	1.121
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
350	7.3532E-07	2.7520E-09	EMVNEG	90	1.4205E-10	3.2639E-01	3.7152E-03	7.3639E-33	1.1095E-04
		DTPP	EMVPOS	90	1.-L-ROUND	XIJRN01	XIJRN021	R-RGUND	JFIN
7.8036E-07	2.6154E-07	ETOTAL		6.9792E-03	2.2659E-01		8.4802E-01	1.1820E-01	1.121
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
375	8.0053E-07	2.8554E-09	EMVNEG	94	1.4203E-10	3.6079E-01	3.7859E-03	7.328E-33	1.1099E-04
		DTPP	EMVPOS	94	1.-L-ROUND	XIJRN01	XIJRN021	R-RGUND	JFIN
7.8143E-07	2.6656E-07	ETOTAL		6.9766E-03	2.2698E-01		8.4802E-01	1.1820E-01	1.121
CYCLE	TIME	DTNH	JSTAR	JPMAX	PMAX	XJPMAX	MYPULSE	MYPREC	MOMENTUM
400	8.5479E-07	2.7509E-09	EMVNEG	97	1.4201E-10	3.9352E-01	3.9645E-03	7.1471E-33	1.1112E-04
		DTPP	EMVPOS	97	1.-L-ROUND	XIJRN01	XIJRN021	R-RGUND	JFIN
7.8266E-07	2.7016E-07	ETOTAL		6.9855E-03	2.3621E-01		8.4802E-01	1.1820E-01	1.121

CYCLE	TIME	JSTAR	JPMAX	P ^{MAX}	MOMENTUM		MOMENTUM	MOMENTUM
					DINH	EMVNEC	EMVPOS	EMVNEG
425	9.1265E-07	1.9110E-09	1.1	1.4200E-10	4.2179E-01	3.967E-03	7.1671E-03	1.1116E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.8422E-07	2.7935E-07	2.3460E-09	-5.9131E-01	1.1124E-04	6.9722E-03	2.2699E-01	6.4894E-01	1.1820E-01
CYCLE	TIME	DINH	JSTAR	JPMAX	P ^{MAX}	MOMENTUM	MOMENTUM	MOMENTUM
450	9.7051E-07	1.9111E-09	1.04	1.4193E-10	4.5349E-01	4.0805E-01	7.0845E-03	1.1114E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.8638E-07	2.8740E-07	2.3456E-09	-7.9253E-01	1.1114E-04	6.0697E-03	2.2697E-01	6.4893E-01	1.1820E-01
CYCLE	TIME	DINH	JSTAR	JPMAX	P ^{MAX}	MOMENTUM	MOMENTUM	MOMENTUM
475	1.02268E-06	1.9111E-09	1.04	1.4196E-10	4.5900E-01	4.3044E-01	6.4653E-03	1.1117E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.88699E-07	3.0336E-07	2.3473E-09	-9.7331E-01	1.1116E-04	6.9668E-03	2.2697E-01	6.4892E-01	1.1820E-01
CYCLE	TIME	DINH	JSTAR	JPMAX	P ^{MAX}	MOMENTUM	MOMENTUM	MOMENTUM
500	1.0791E-06	1.9109E-09	1.11	1.4193E-10	4.5152E-01	4.3250E-01	6.4571E-03	1.1117E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.98856E-07	3.0543E-07	2.3467E-09	-1.1225E-02	1.1117E-04	5.9629E-03	2.2697E-01	6.4891E-01	1.1820E-01
CYCLE	TIME	DINH	JSTAR	JPMAX	P ^{MAX}	MOMENTUM	MOMENTUM	MOMENTUM
525	1.1281E-06	2.7514E-09	1.14	1.4181E-10	5.2948E-01	4.6625E-01	7.1477E-03	1.1230E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.9044E-07	2.6648E-07	2.3460E-09	-1.2173E-02	1.1119E-04	5.9607E-03	2.2696E-01	6.4887E-01	1.1820E-01
CYCLE	TIME	DINH	JSTAR	JPMAX	P ^{MAX}	MOMENTUM	MOMENTUM	MOMENTUM
550	1.1842E-06	1.9114E-09	1.19	1.4142E-10	5.5900E-01	4.1267E-01	7.0985E-03	1.1225E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.9373E-07	2.9180E-07	2.3451E-09	-1.3342E-02	1.1120E-04	5.9622E-03	2.2696E-01	6.4883E-01	1.1820E-01
CYCLE	TIME	DINH	JSTAR	JPMAX	P ^{MAX}	MOMENTUM	MOMENTUM	MOMENTUM
554	1.1918E-06	1.9109E-09	1.15	1.4135E-10	5.7446E-01	4.4554E-01	6.7543E-03	1.1212E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.9371E-07	3.1459E-07	2.3452E-09	-1.4710E-02	1.1212E-04	6.9620E-03	2.2696E-01	6.4898E-01	1.1820E-01
CYCLE	TIME	DINH	JSTAR	JPMAX	P ^{MAX}	MOMENTUM	MOMENTUM	MOMENTUM
575	1.2503E-06	2.8661E-09	1.99	1.4135E-10	5.7446E-01	4.4554E-01	6.7543E-03	1.1212E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.9273E-07	3.1459E-07	2.3378E-09	-1.0533E-02	1.1116E-04	6.9620E-03	2.2696E-01	6.4898E-01	1.1820E-01
CYCLE	TIME	DINH	JSTAR	JPMAX	P ^{MAX}	MOMENTUM	MOMENTUM	MOMENTUM
575	1.2503E-06	2.8661E-09	1.01	1.4123E-10	6.0763E-01	4.5852E-01	6.6212E-03	1.1212E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.9273E-07	3.2467E-07	2.3396E-09	-1.3715E-02	1.1200E-04	6.9592E-03	2.2696E-01	6.4949E-01	1.1820E-01
CYCLE	TIME	DINH	JSTAR	JPMAX	P ^{MAX}	MOMENTUM	MOMENTUM	MOMENTUM
600	1.3187E-06	2.8661E-09	1.01	1.4052E-10	6.4356E-01	4.5625E-01	6.6727E-03	1.1212E-02
DTPP	DTPULS	ETOTAL	EMVNEC	L-BGND	X1J84011	X1J84011	X1J84011	X1J84011
7.9952E-07	3.2468E-07	2.3384E-09	-1.5598E-02	1.1219E-04	6.9552E-03	2.2696E-01	6.4949E-01	1.1820E-01

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13. ABSTRACT

The report describes the one-dimensional Lagrangian hydrodynamics computer program, PUFF. The code is used primarily in the study of X-ray effects. In the past year, it has been extensively revised and is now quite different from versions used outside the Air Force Weapons Laboratory. The major calculations in each subroutine are explained with a complete description of all input-output variables. Sample problems with the appropriate data deck are included to allow a user to become familiar with data arrangement and to check the program on his computer.

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Security Classification

14 KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Hydrodynamics Calculations One-dimensional Fluid Flow X-ray Effects Code One-dimensional Hydrodynamic Program PUFF Code - Energy deposition P PUFF Code - Plate slap						
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AIR FORCE WEAPONS LABORATORY
Air Force Systems Command
Kirtland Air Force Base
New Mexico

6 July 1965

ERRATA

AFWL TR-65-24

THE PUFF AND P PUFF COMPUTER PROGRAMS
Unclassified report, March 1965

When the P PUFF Fortran listing is updated with
the Addendum changes, JPMAXI must be added to
each of the COMMON blocks.

On page 18 the 5th variable defined should read
NRZC instead of NRZ.

Authority:

RALPH H. PENNINGTON
Lt Colonel, USAF
2 July 1965

C. W. Haig
C. W. HAIG
Chief, Reports and Data Branch
Technical Information Division

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Research and Technology Division
AIR FORCE WEAPONS LABORATORY
Air Force Systems Command
Kirtland Air Force Base
New Mexico

SET 5, 1963

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28 May 1965

ADDENDUM

AFWL TR-65-24

THE PUFF AND P PUFF COMPUTER PROGRAMS

This addendum is to notify users of recent improvements and changes to the PUFF and P PUFF programs and to correct two minor discrepancies in AFWL TR-65-24.

The improvements are related mostly to REZONE and should help to improve pulse resolution in poorly zoned problems. The major changes are found in the Equation of State Subroutine. The solid phase equation of state is now fit to raw Hugoniot data.

These additions will affect the solutions to the three sample problems slightly. If one wishes to check the code conversion to his computer, we suggest adding the following changes after the initial conversion has been checked.

On page 23, delete the first statement past statement number 17, SSCK=1..

On page 24, delete statement number 53 and substitute the following three statements:

GO TO 531
53 SSCK=1.
531 DTN=DTNH .

On page 31, change the first statement before statement number 2,

IF(JPMAX-JZPUL-JRZL-JPMAXI) 87, 87, 2

to read

IF(JPMAX-JZPUL-JPMAXI) 87, 87, 2 .

On page 33, delete statement number 50 and one statement past, JRZV=1 and MRZ=1. Number the next statement, JFINO=JFIN, 50; 50 JFINO=JFIN.

Change the second statement on page 34 to M=1 .

On page 34, delete the first statement past statement number 52 and substitute the following four statements:

```
IF(TIME-SDUR) 520, 530, 530  
520 NRZ=1  
GO TO 53  
530 IF(JPLC-JV-JRZL) 53, 53, 60 .
```

On page 34, change the first statement before statement number 56 to read

```
IF(JPLC+1-JBND(MM)) 57, 56, 56 .
```

On page 35, delete the second statement past statement number 86, NRZ=N, and substitute the following three statements:

```
IF(JPMAXI) 860, 860, 870  
860 JPMAXI=0  
870 NRZ=N .
```

On page 38, change statement number 7 and one statement past to read

```
7 TS2=(CUSP1(M)+((CUSPS(M)*ARG+CUSPD(M))*ARG  
+CUSPC(M))*ARG)*(1.-(CUSPG(M)*EMU)/2.)  
P1=TS2+CUSPG(M)*D*E1,
```

and change statement number 8 to read

```
8 TS2 = ((EQSTS(M)*EMU+EQSTD(M))*EMU+EQSTC(M))  
*EMU*(1.-(EQSTG(M)*EMU)/2.) .
```

On page 41, delete statement number 20 and substitute the following three statements:

```
20 IF(N-1) 200, 200, 210  
200 JPMAXI=JPMAX+10  
210 IF(J-JSTAR) 22, 21, 21 .
```

On page 44, change the second statement past statement number 31, NRZ=-50, to read NRZ=50.

On page 46, change the first statement before statement number 2 to read

```
IF(JPMAX-JPMAXI) 85, 85, 2 .
```

On page 48, change the first statement before statement 54 to read

```
IF(JPLC+i-JBND(MM))55, 54, 54 .
```

On page 50, delete the first statement past statement number 84, NRZ=N, and substitute the following four statements:

```
JPMAXI=JPMAXI-JRZ  
IF(JPMAXI) 840, 840, 850  
840 JPMAXI=0  
850 NRZ=N .
```

On page 53, delete the first executable statement, ENU=D/RHO(M), and substitute the following five statements:

```
IF(El) 10, 10, 20
10 El=0.
P1=0.
GO TO 9
20 ENU=D/RHO(M).
```

Also, there are two more changes on page 53. Statement number 7 and one statement past are changed to

```
7 TS2=(CUSP1(M)+((CUSPS(M)*ARG+CUSPD(M))*ARG
      +CUSPC(M))*ARG)*(1.-(CUSPG(M)*EMU)/2.)
P1=TS2+CUSPG(M)*D*El,
```

and statement number 8 is changed to

```
8 TS2=((EQSTS(M)*EMU+EQSTD(M))*EMU+EQSTC(M))*EMU*(1.-(EQSTG(M)*EMU)/2.).
```

This addendum has been reviewed and is approved.

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